

UNH – CCTVAL Collaboration on Cryogenic Fridge Design and Simulation

TEAM WORK USM:

WILLIAM BROOKS

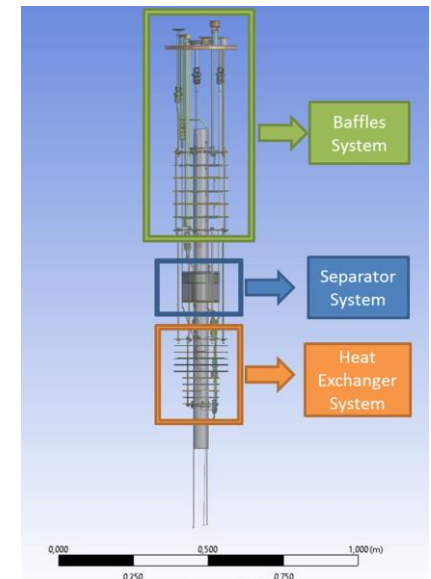
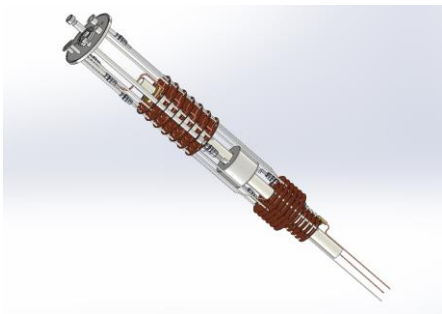
DAVID ALIAGA

PABLO BUNOUT

TEAM WORK UNH : KARL SLIFER

NATHALY SANTIESTEBAN

ELENA LONG





Cryogenic Fridge Modeling



General Goals

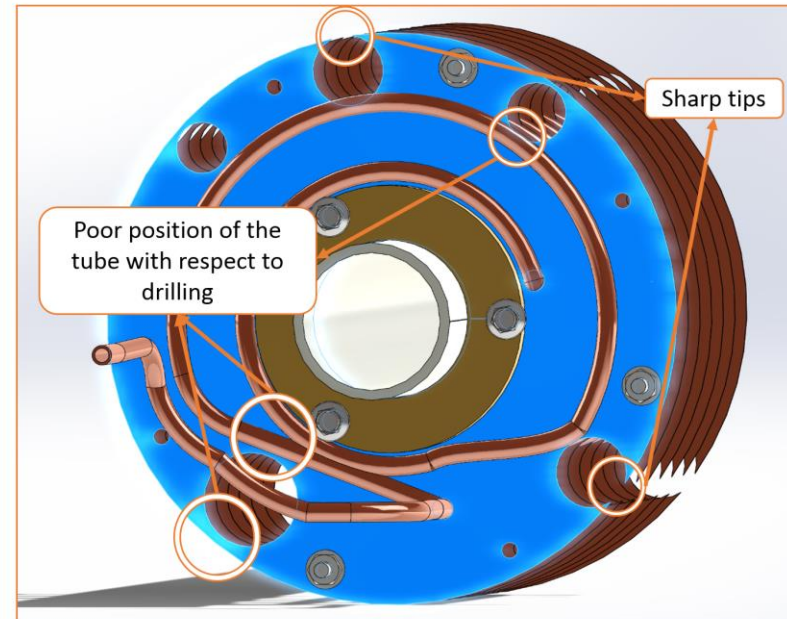
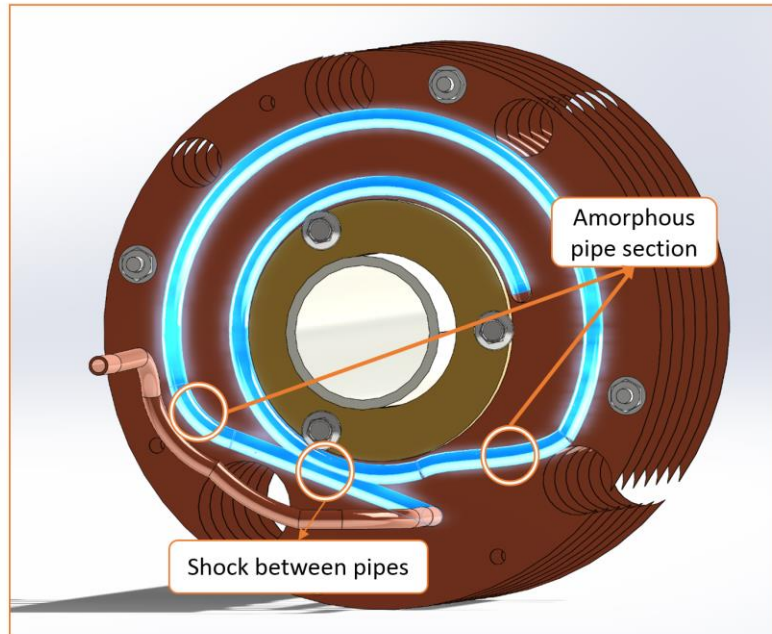
- 1. Design strategy to simulating
- 2. Analysis of theoreticals and numericals models to physical problems
- 3. Make CAD models of devices to simulating
- 4. Performs first group of simulations

Problems in design found (baffles system)

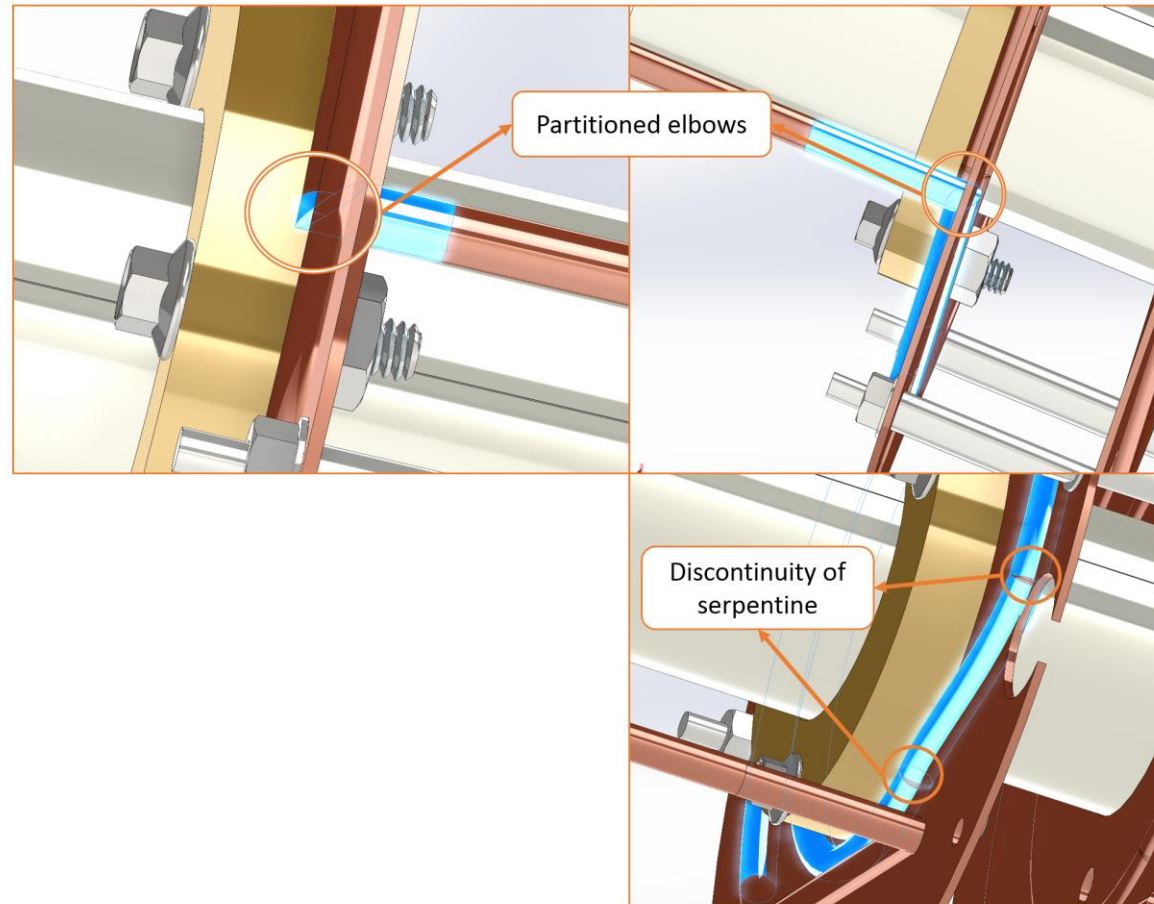
- 1. Design problems to construction
- 2. Design problems to generate meshing in simulation softwares



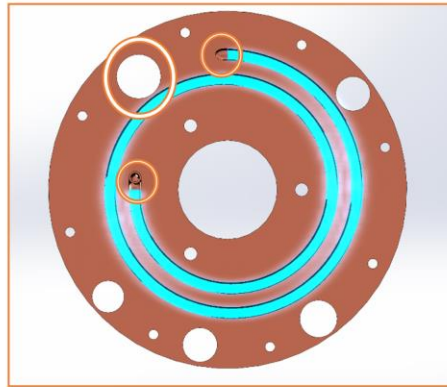
Baffles & HE Modeling : Baffle and HE Geometrical Details



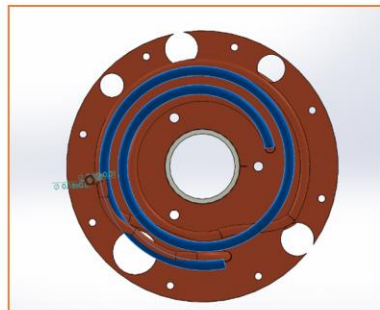
Baffles & HE Modeling : Baffle and HE Geometrical Details



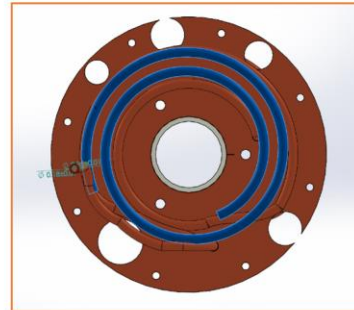
Baffles & HE Modeling : Baffle and HE Geometrical Details



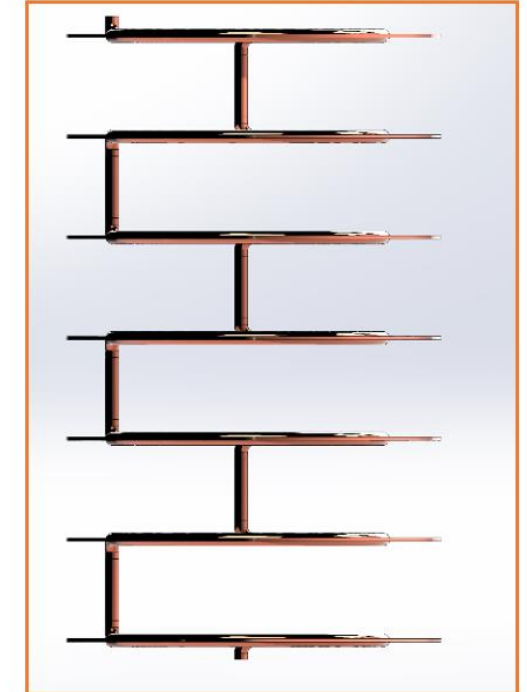
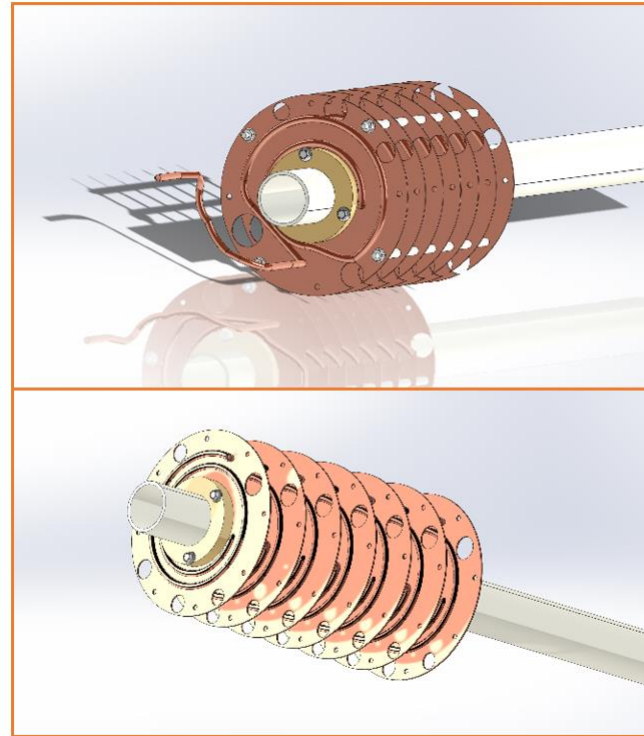
Rotation of pipe position
with respect drilling in
baffle



Actually position of
pipe with respect baffle



New position of pipe
with respect baffle

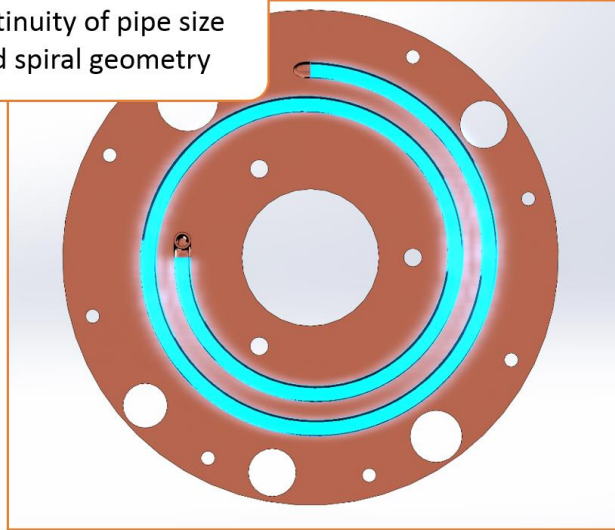




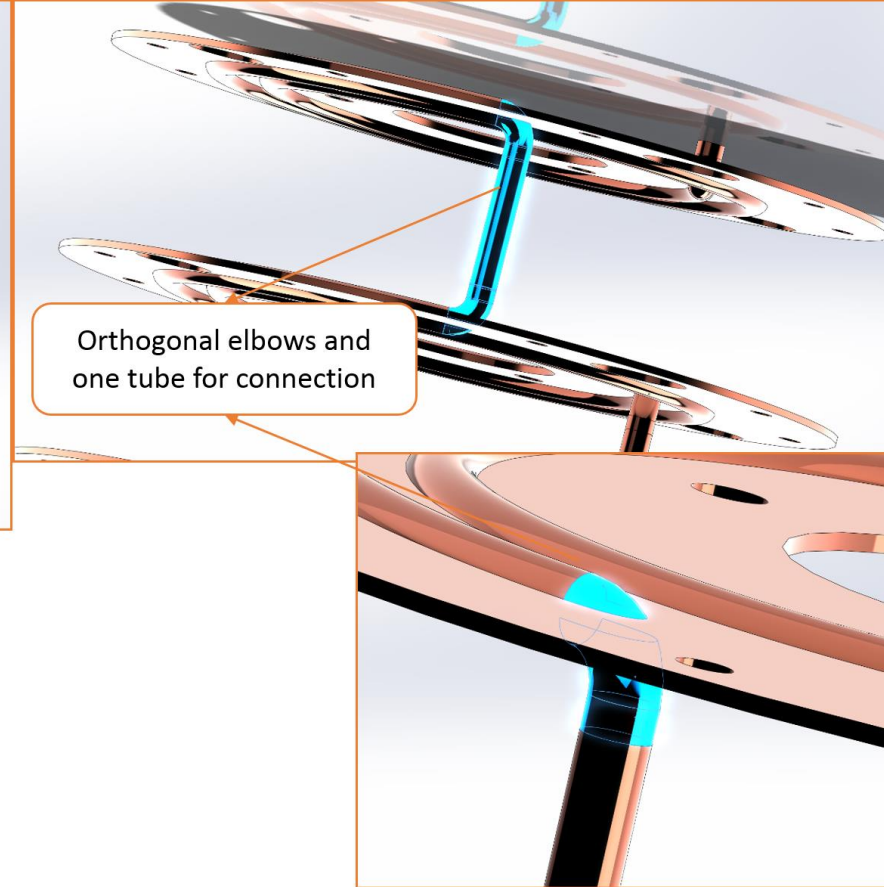
Baffles & HE Modeling : Baffle and HE geometrical modifications



Continuity of pipe size
and spiral geometry

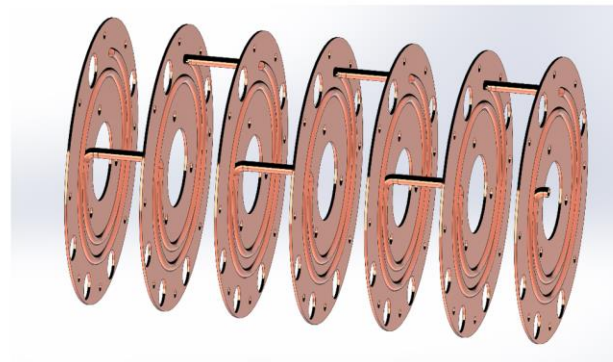
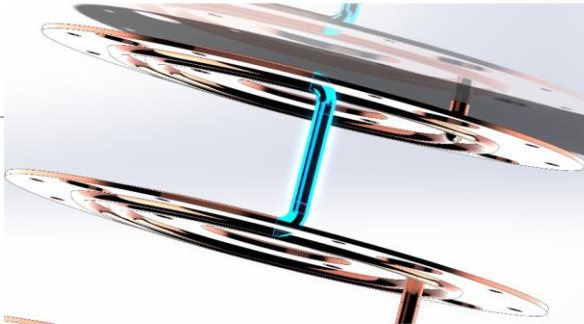
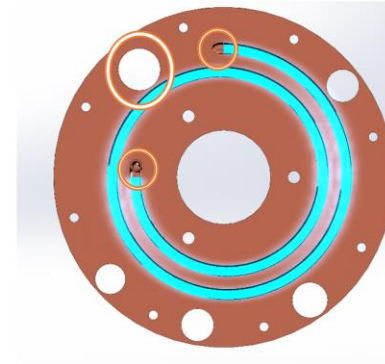
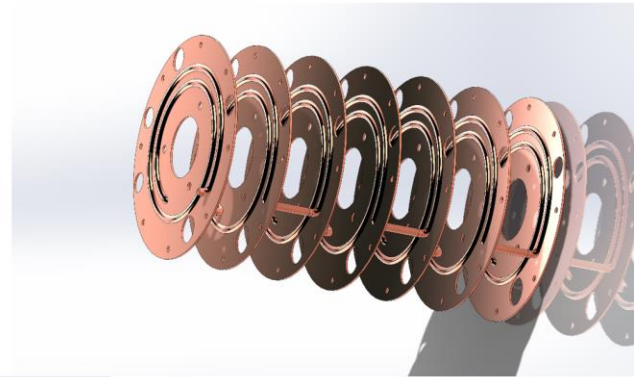
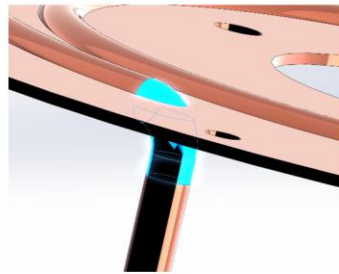


Orthogonal elbows and
one tube for connection



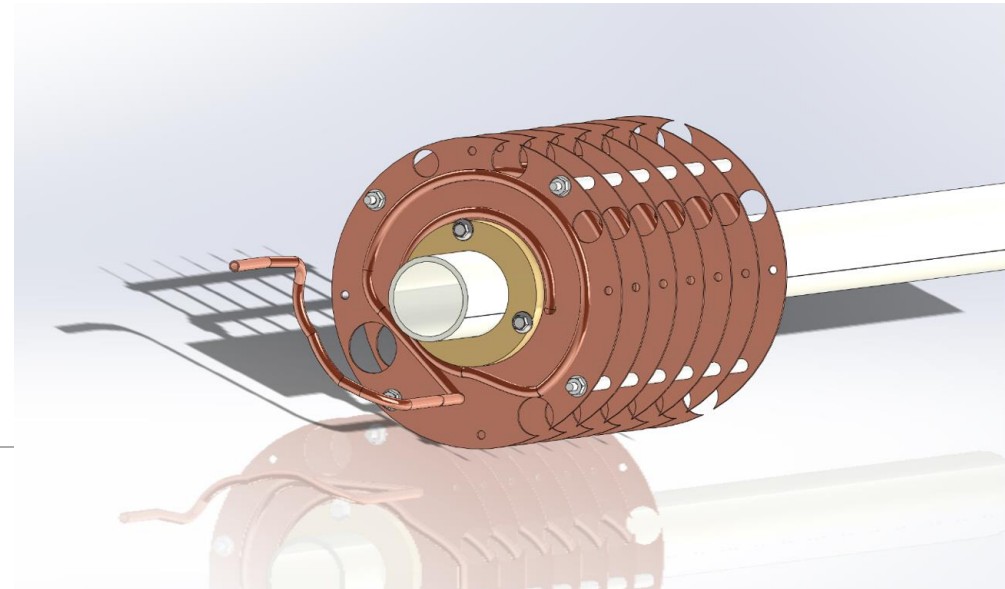
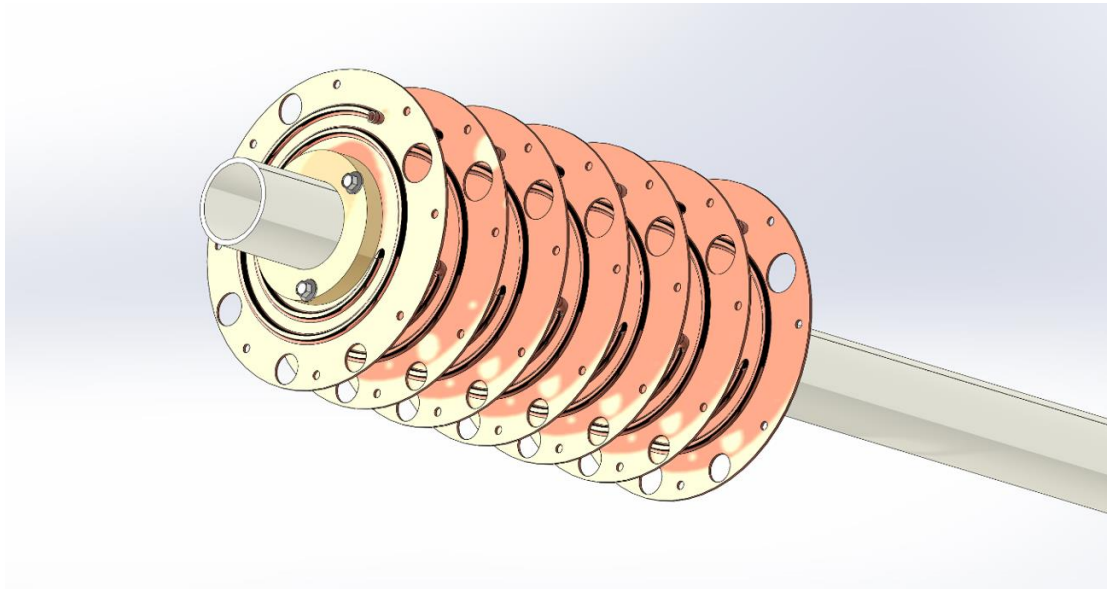


Baffles & HE Modeling : Baffle and HE geometrical modifications





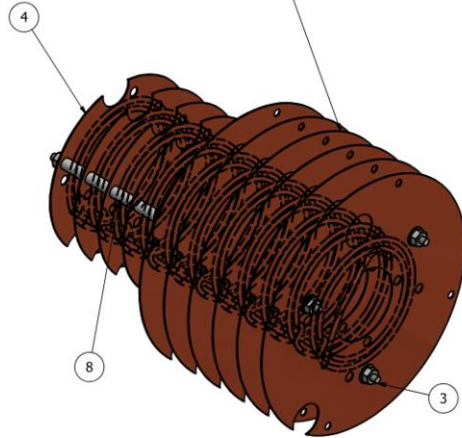
Baffles & HE Modeling : Baffle and HE geometrical
modifications



Baffles & HE Modeling : Material Thermal Properties

- Cooper C10200 (ASTM B152) (Oxygen Free 0,001% max)

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NUCLEAR PHYSICS GROUP

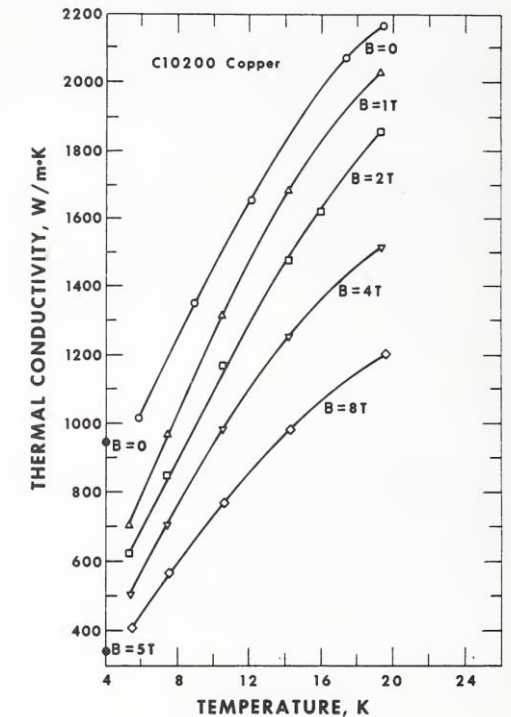
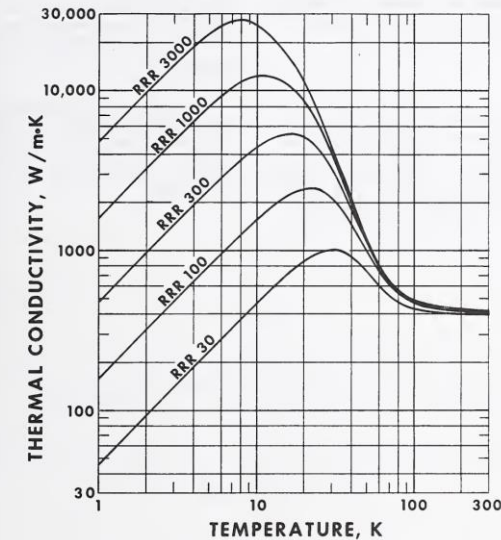
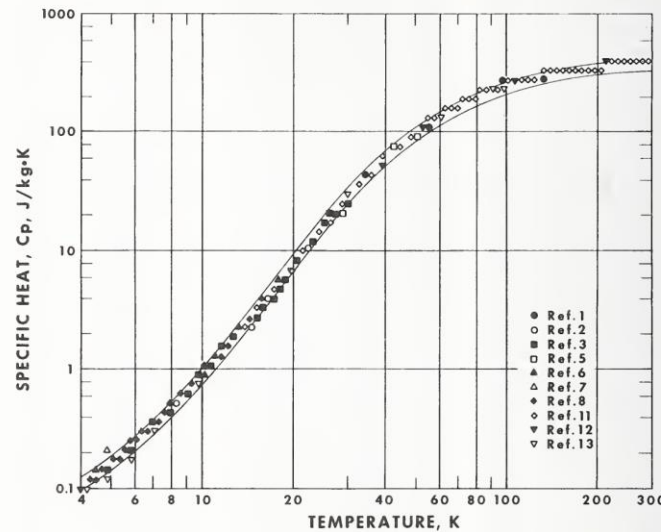


PARTS LIST			
ITEM	QTY	PART NUMBER	MATERIAL
1	6	NPG-1000-0054	C102 Copper
2	6	91343A104	SST 316
3	3	NPG-1000-0006	SST 316
4	5	NPG-1000-0055	C102 Copper
5	1	NPG-1000-0019	Aluminum
6	4	91720A197	SST 316
7	4	90205A309	SST 316

[1]

WROUGHT ALLOYS										
ALLOY NO.	DESIG-NATION	DESCRIPTION	Cu (Incl. Ag) (% Min)	Ag		As	Sb	P	Te	OTHER NAMED ELEMENTS
				% Min	Troy Oz Min					
C10200 (c)	OF	Oxygen Free	99.95	—	—	—	—	—	—	—

(c) These are high conductivity coppers which have in the annealed condition a minimum conductivity of 100% IACS.

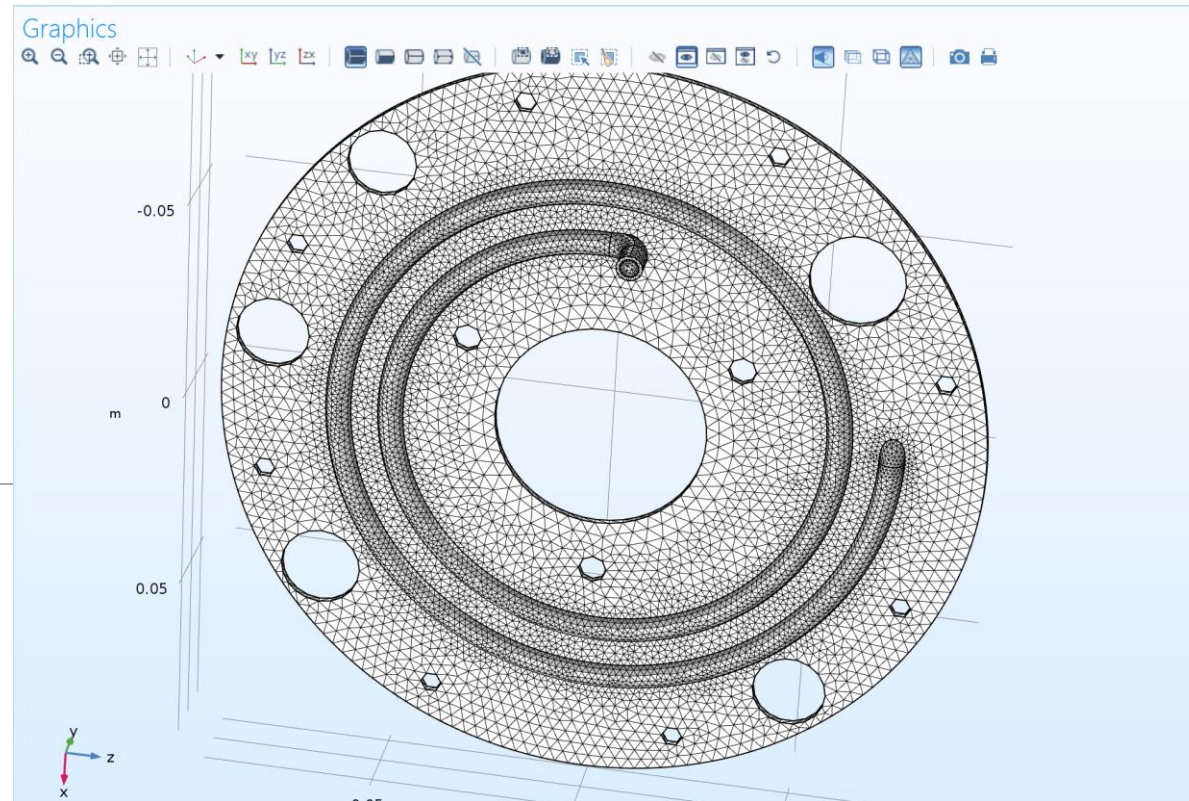


[1] Simon, N, J., Drexler , E, S., Reed, R, P., 1992. Properties of Copper and Copper Alloys at Cryogenic Temperatures. NIST Monograph 177.

Mesh Domain

Mesh Statistics :

Mesh consists of 278.753 elements. Minimum quality: 0.1106; average quality: 0.6606.



Fluid and Solid Domain (Helium Gas & Copper)

Laminar Incompressible Flow Solver

Inlet: 5 SLPM

Outlet = Open Boundary ;

Wall = no slip

Heat Transfer fluid-solid Solver

Inlet: $T = 4.2 \text{ K}$

Outlet = Open Boundary ;

Thermal Insulation BC

Initial Conditios: Fluid@ $T=5 \text{ K}$

Baffle @ $T = 77 \text{ K}$

▼ Boundary Condition

Mass flow

▼ Mass Flow

Mass flow type:

Standard flow rate

Standard flow rate defined by:

Standard pressure and temperature

Standard flow rate:

Q_{sv} m^3/s

Standard pressure:

P_{st} Pa

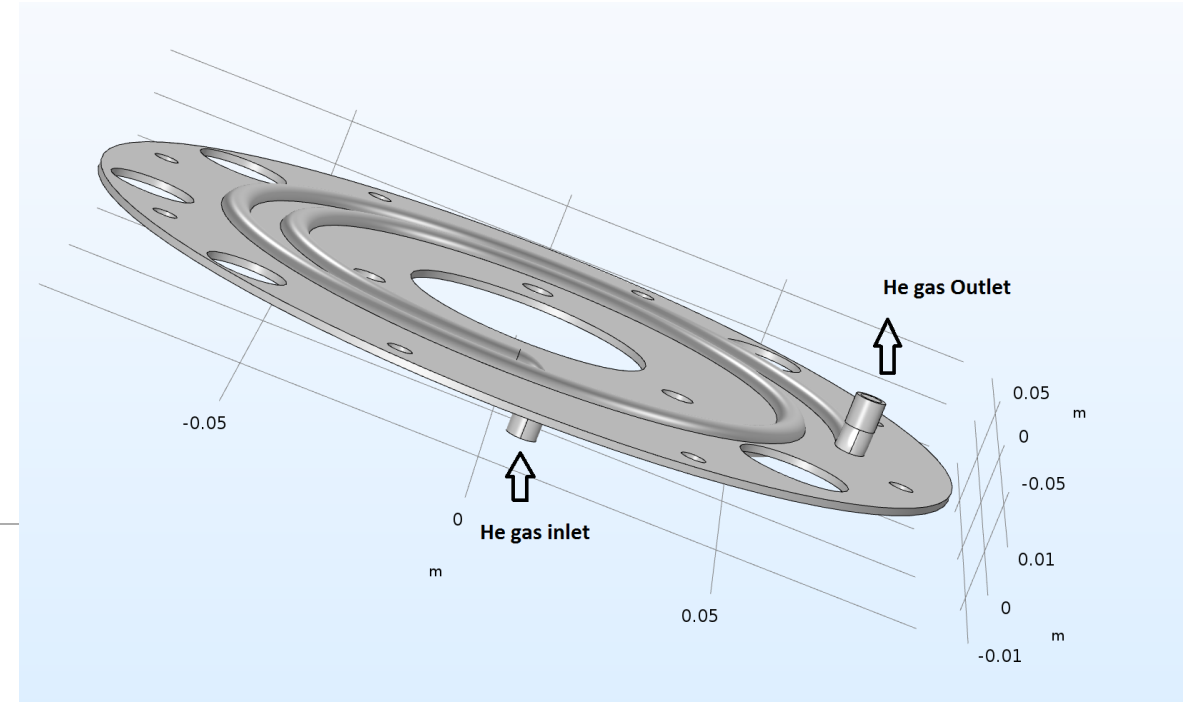
Standard temperature:

T_{st} K

Mean molar mass:

M_n

kg/mol

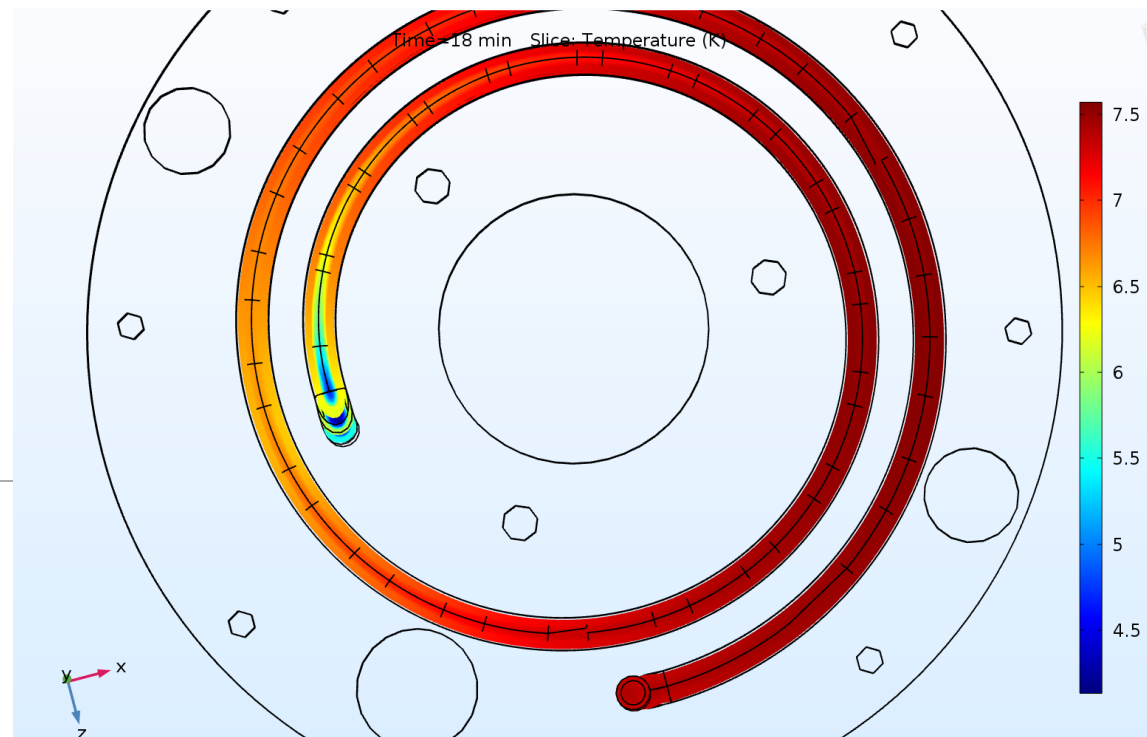
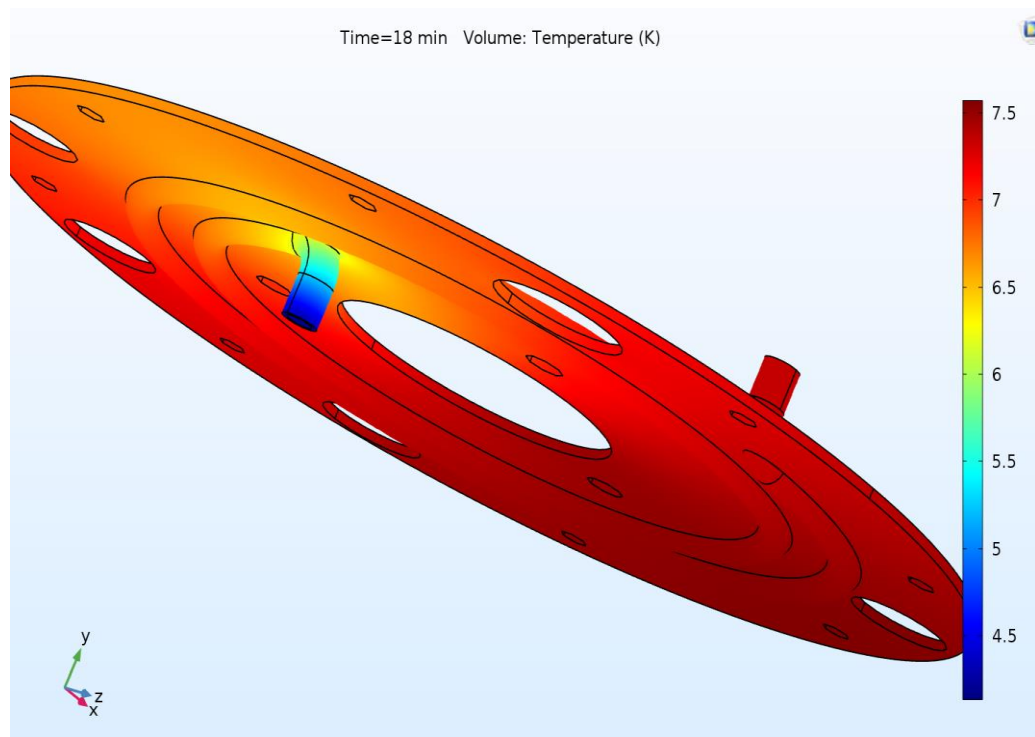


Linear System of 290.440 DOF

Time-dependent solver (BDF)
Number of degrees of freedom solved for: 290440 (plus 50445 internal DOFs).

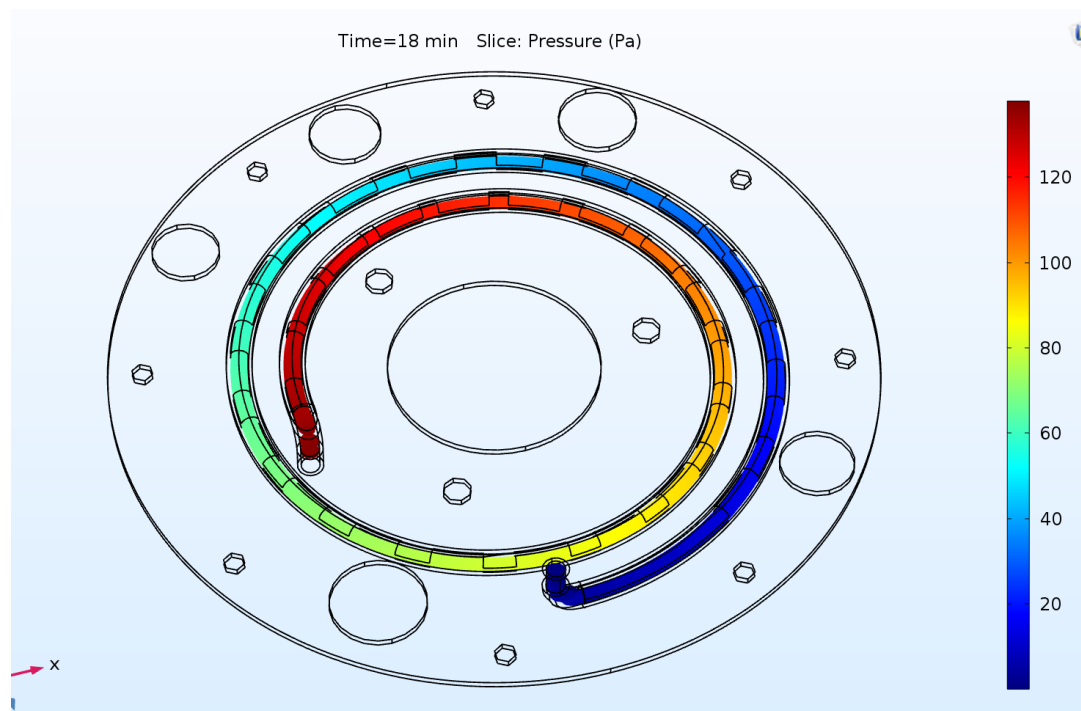
Last computation time:
14 min 37 s

Temperature

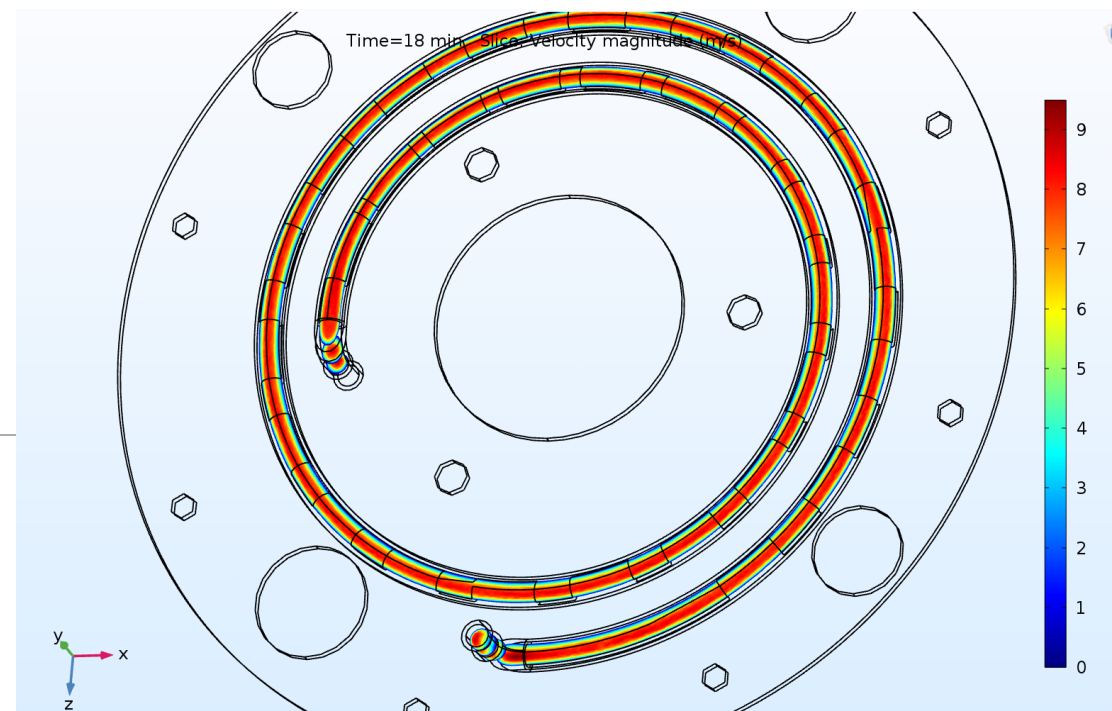


Baffles & HE Modeling : Results

Pressure



Velocity



- First Evaporation Fridge Cool-Down

2015-09 Cool Down Analysis

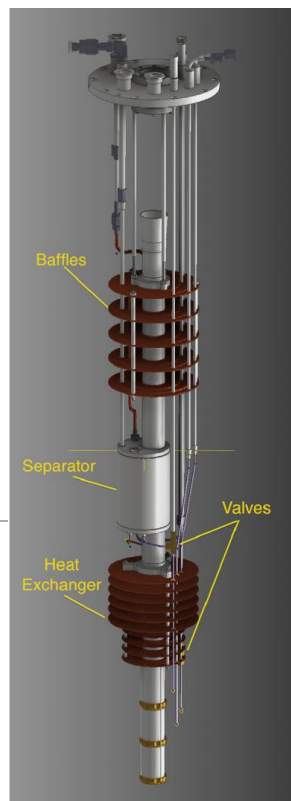
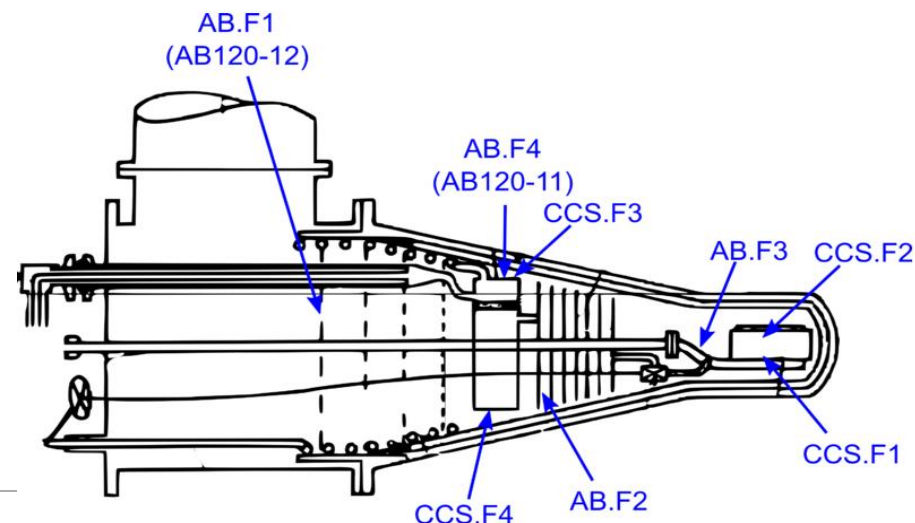


Fig. 3. The 1 K evaporation refrigerator.



[4]

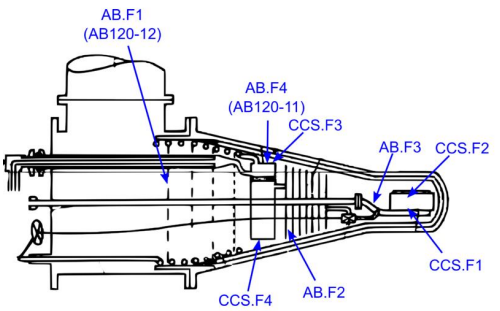
[3]

[3] Pierce,j., Maxwell,J., Badman,T. et all . 2014. Dynamically polarized target for the g2p and GEp experiments at Jefferson Lab. Nuclear Instruments and Methods in Physics Research A738 54-60.

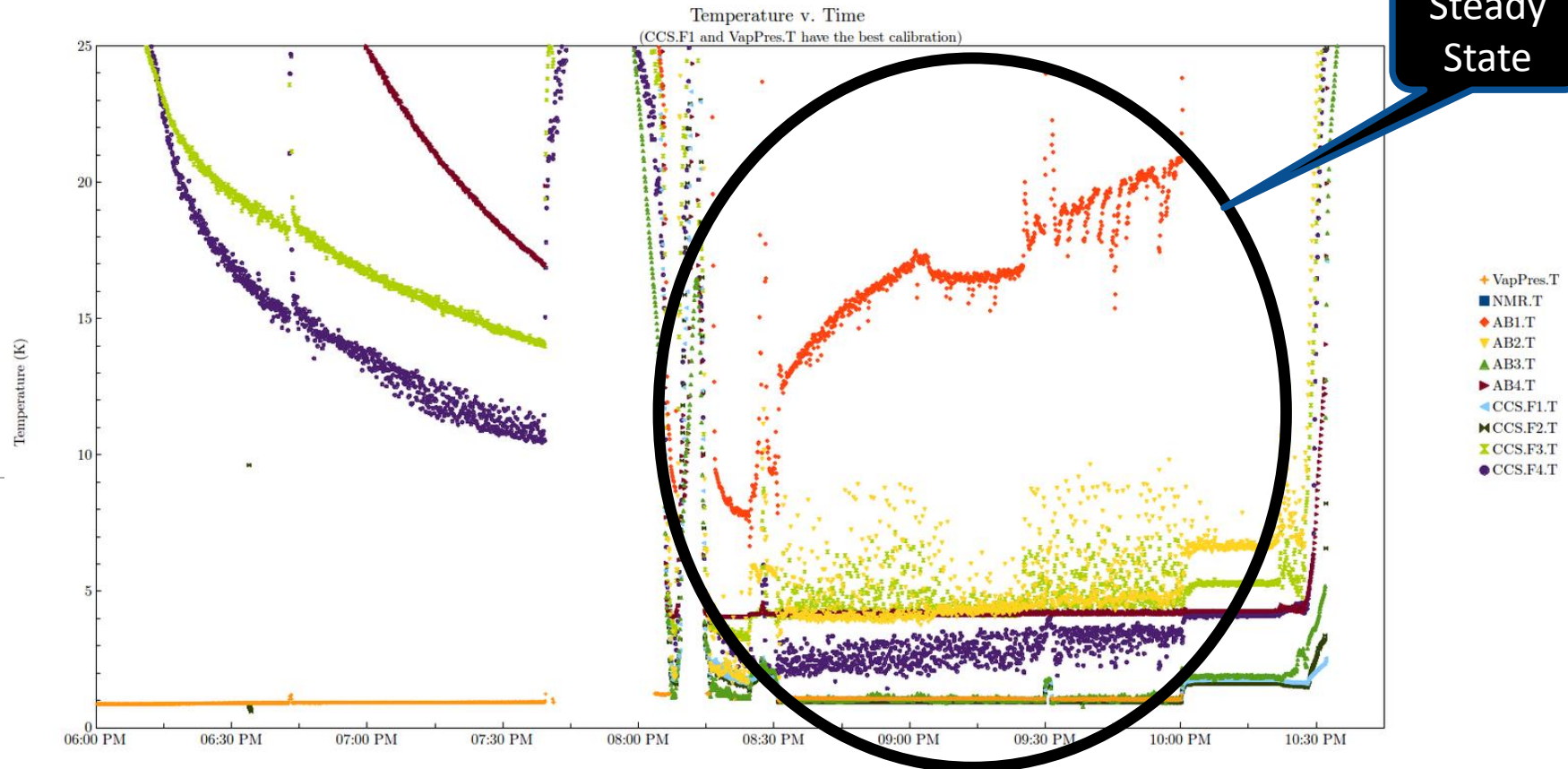
[4] UNH-NPG http://nuclear.unh.edu/wiki/index.php?title=2015-09_Cool_Down_Analysis

- First Evaporation Fridge Cool-Down

Steady
State



[4]





Baffles & HE Modeling : Operation Curve



- First Evaporation Fridge Cool-Down

• VapPres.T
• NMR.T
• ABL.T
• AB2.T
• ABL.T
• CCS.F1.T
• CCS.F2.T
• CCS.F3.T
• CCS.F4.T

Temperature (K)

06:00 PM

Saturation
Point He-4

Upper
HE

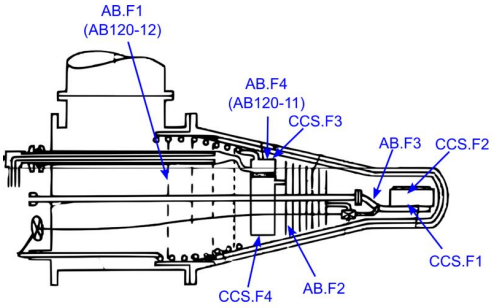
Lhe Inner
Separator

Upper
Baffle

He inlet
separator

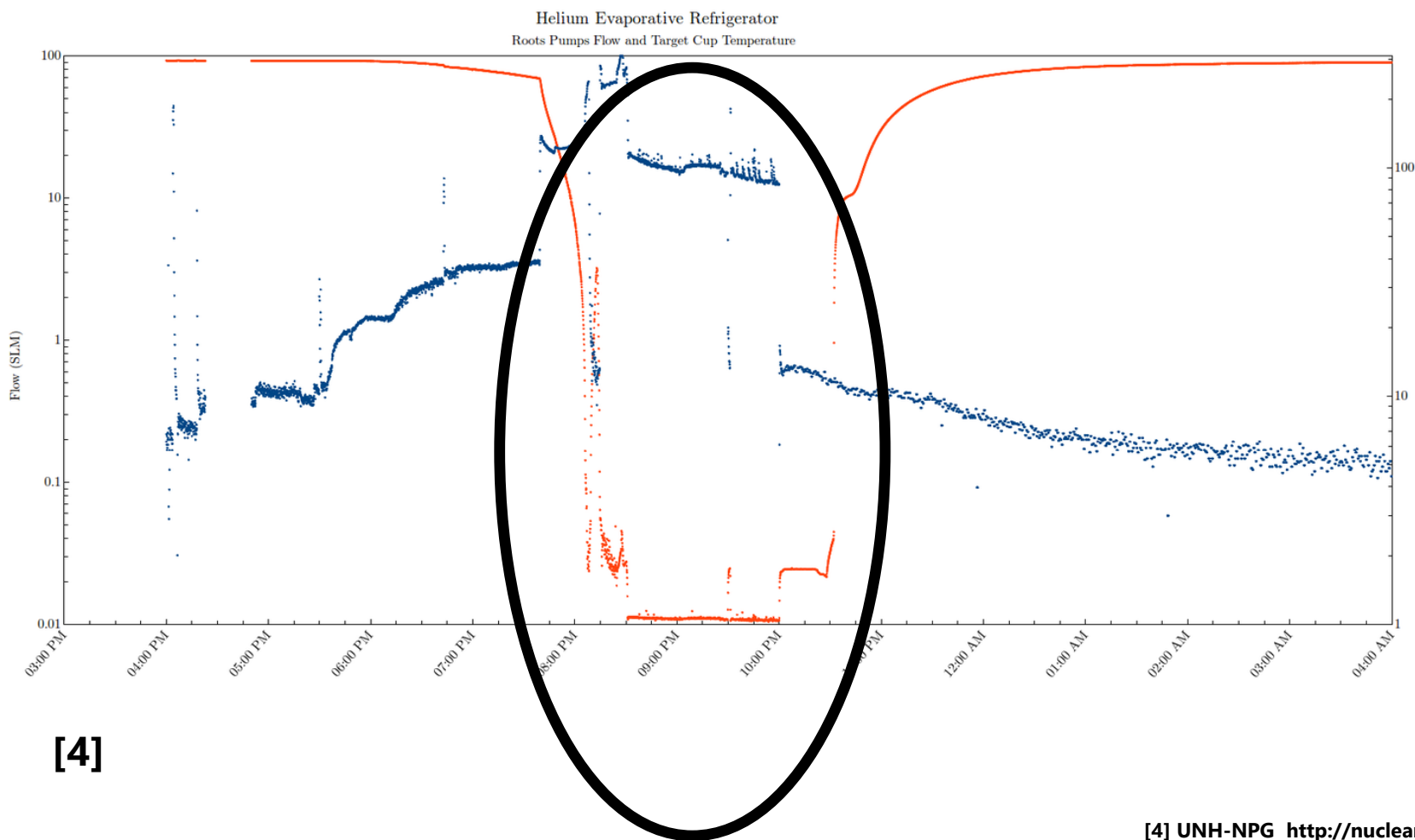
BP & N
Valves

Nose &
lower site



Baffles & HE Modeling: Pumped Helium

- First Evaporation Fridge Cool-Down



$$F[\text{SLPM}] = F[\text{LPM}] \times (294.26 / T_{\text{gas}}) \times (P_{\text{gas}} / 14.696)$$

P_{gas} – Absolute gas pressure in Psia

T_{gas} – Gas Temperature in K

During operation :

$P_{\text{gas}} = 200$ [mtorr] $T_{\text{gas room}} = 300$ K.

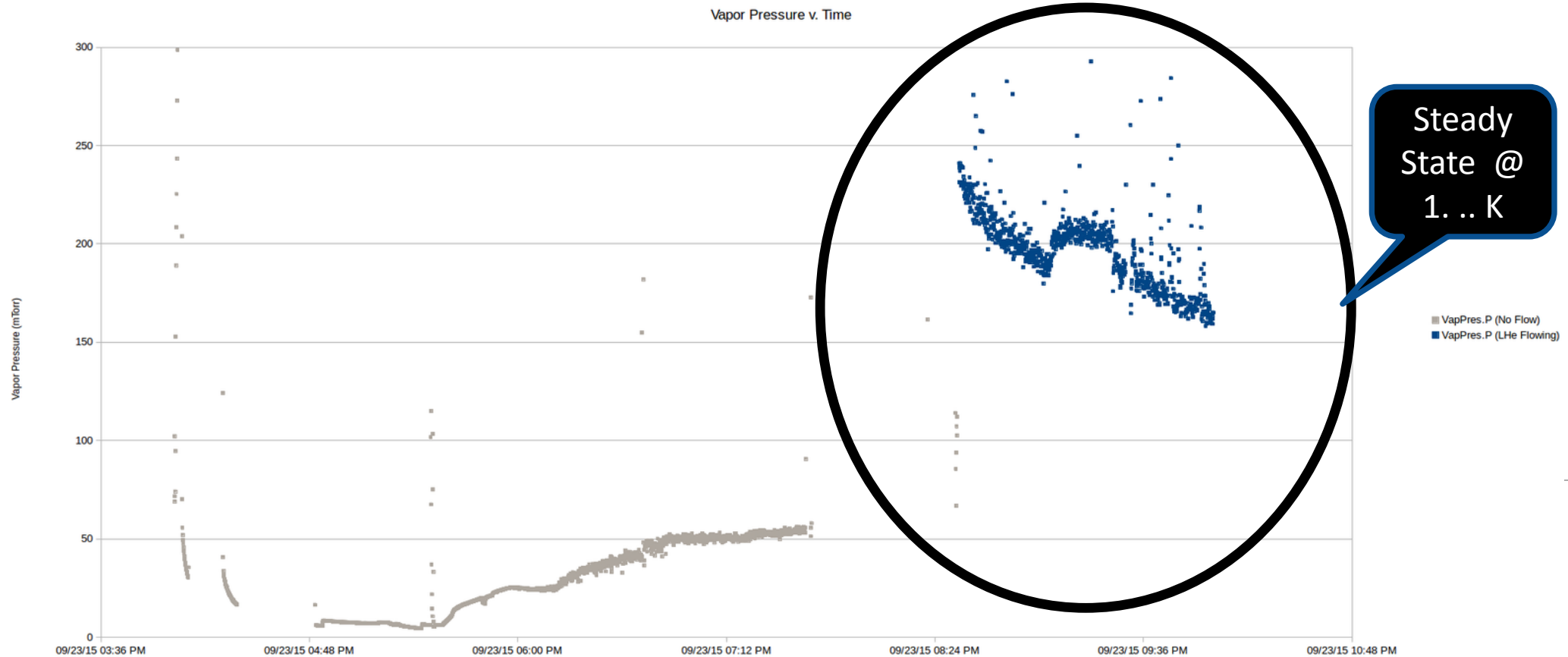
$V = 12$ [SLPM]

3.487 [m³/hr] Root Pumping

[4]

Baffles & HE Modeling: Pumped Helium

- First Evaporation Fridge Cool-Down



[4]

- First Evaporation Fridge Cool-Down

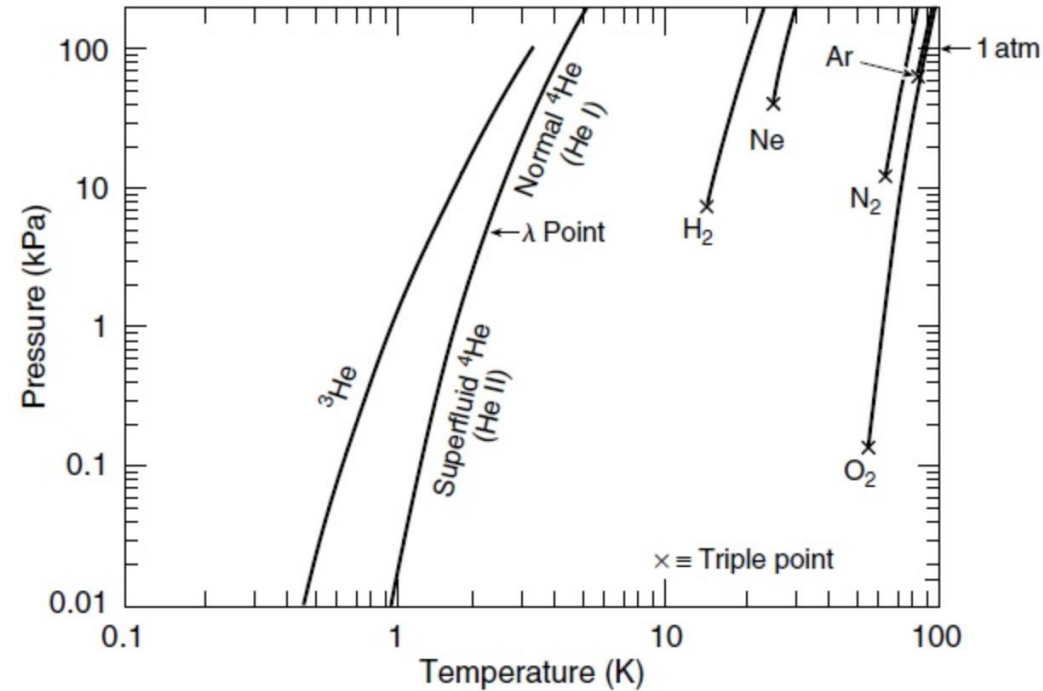
- Pumping liquid helium @ 1 K,

$$\begin{aligned} \text{VP} &= 160 \text{ [ubar]} \\ &= 0.016 \text{ [kPas]} \\ &= 1.2 \text{ E-1 [Torr]} = 120 \text{ [mTorr]} \end{aligned}$$

- Choose Pumping speed
(depends on heat load of system
(0.1 -3 W))

$$H_{\text{evap He @ 1K}} = 80 - 92 \text{ [J/mol]}$$

- Pump speed= $\frac{\text{Heat load}}{H_{\text{evap}}}$
[mol/s] or [m3/hr] --→ by ideal gas
law

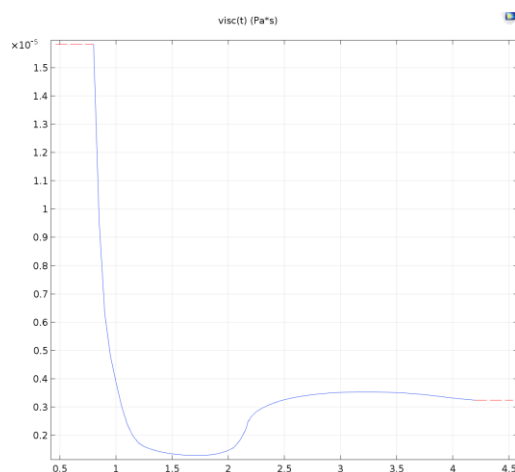


[5]

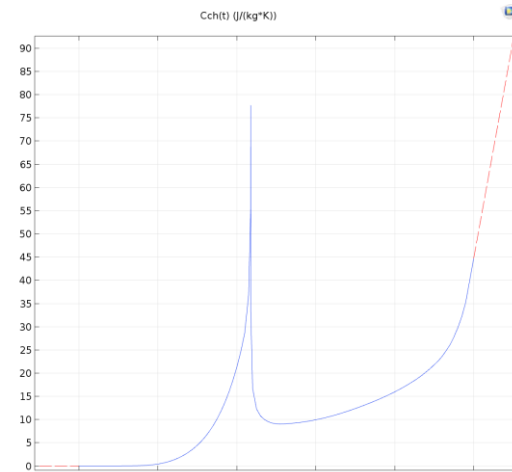
Heat Load Pumped		
pump speed	3487	m3/hr
pump speed	0,97	m3/s
pump speed	968,61	lt/s
R	8,31	Ctant
T	295,00	K
P	26,66	Pa
pump speed	968,61	lt/s
pump speed	0,01	mol/s
heat load	1,23	W
H helium	83	J/mol
for [4.2K- 1.4K]		

[5] Ekin, J, W.2006. Experimental Techniques for Low- Temperature Measurements, Cryostat Designs, Material Properties, and Superconductor Critical- Current Testing. Oxford University Press. p, 673.

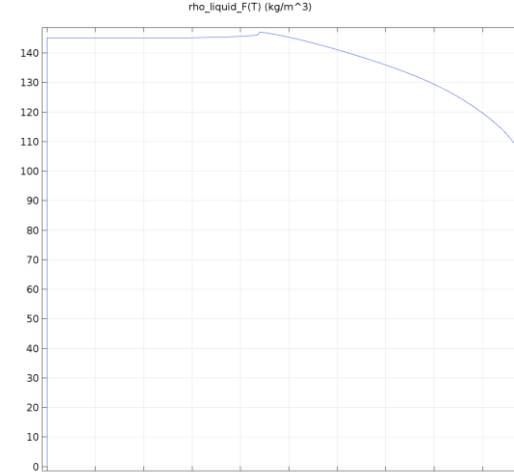
Dynamic Viscosity



Heat Capacity



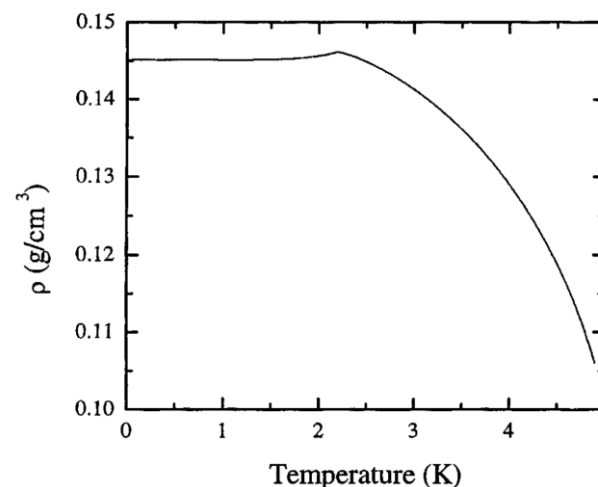
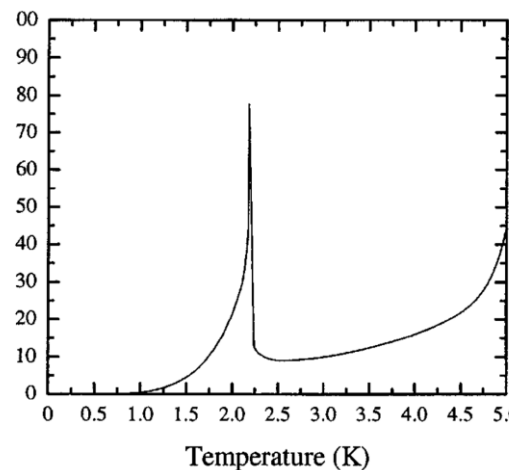
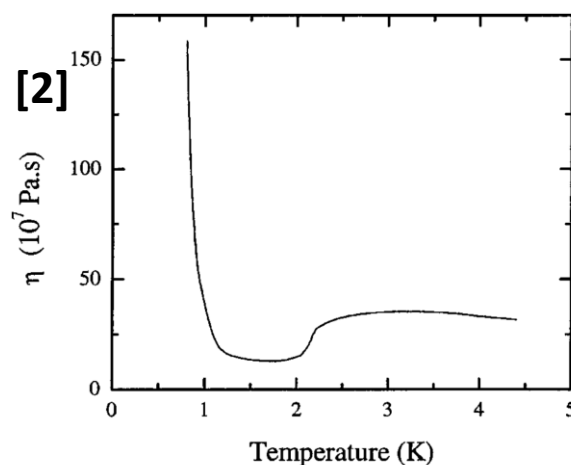
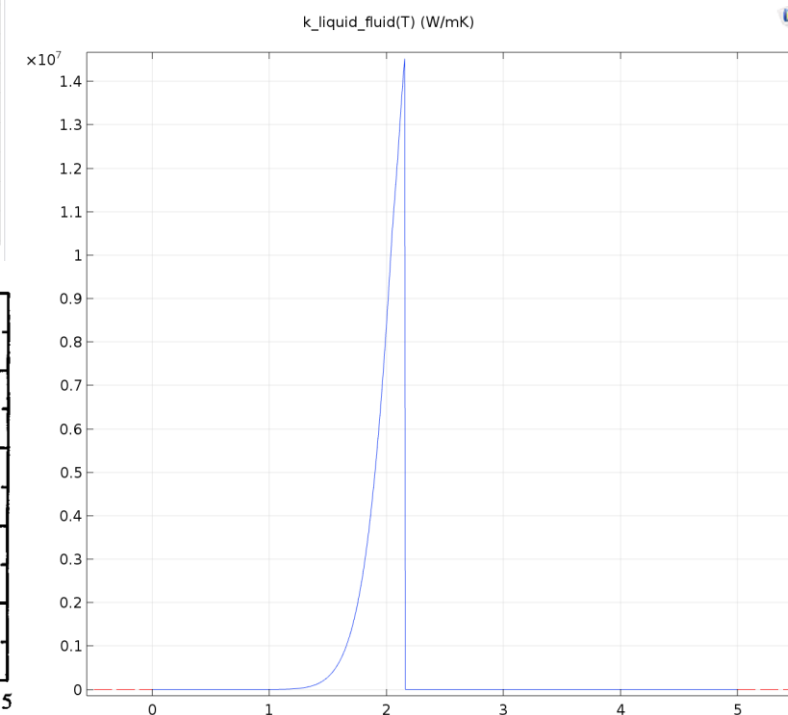
Density



Thermal Conductivity

$$K_{eff} = \frac{\dot{Q}}{\pi R^2 \Delta T} = \frac{R^2}{8\beta^2 T^3 \eta} = \frac{R^2 \rho^2 T S^2}{8\eta}$$

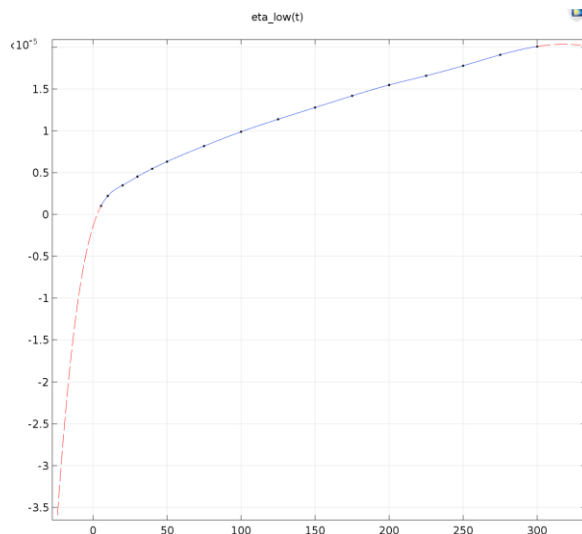
Laminar situation: Landau regime



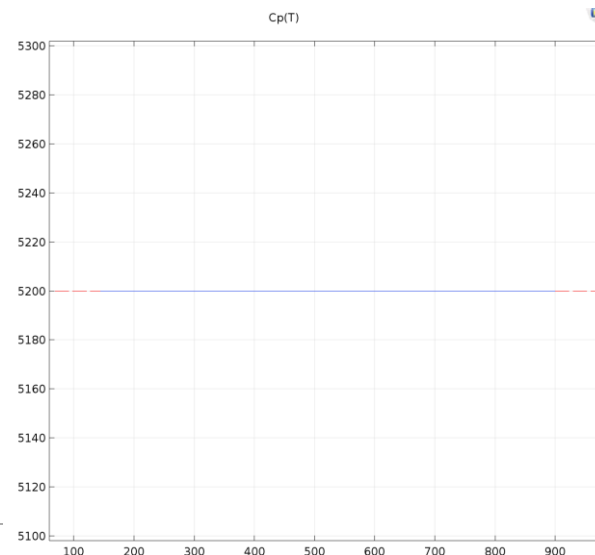
[2] Russell J. Donnelly and Carlo F. Barenghi. 1998. The Observed Properties of Liquid Helium at the Saturated Vapor Pressure, *Journal of Physical and Chemical Reference Data* 27, 1217 (1998)

[3] Sciacca, M. Jou, D. Mongiovi, M. S. 2013. Effective thermal conductivity of helium II: from Landau to Gotter- Mellink regimes. Cornell University Library.

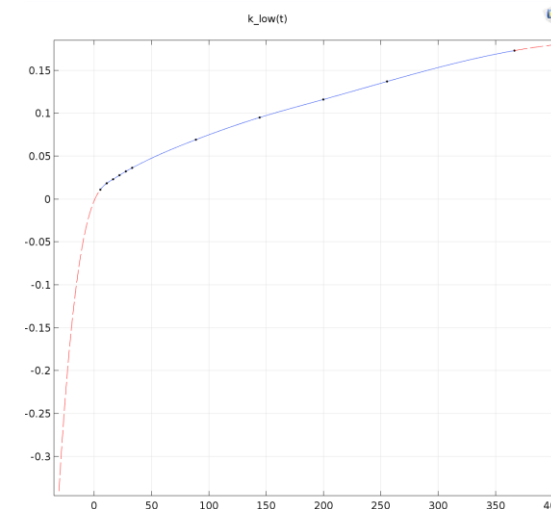
Dinamic Viscosity



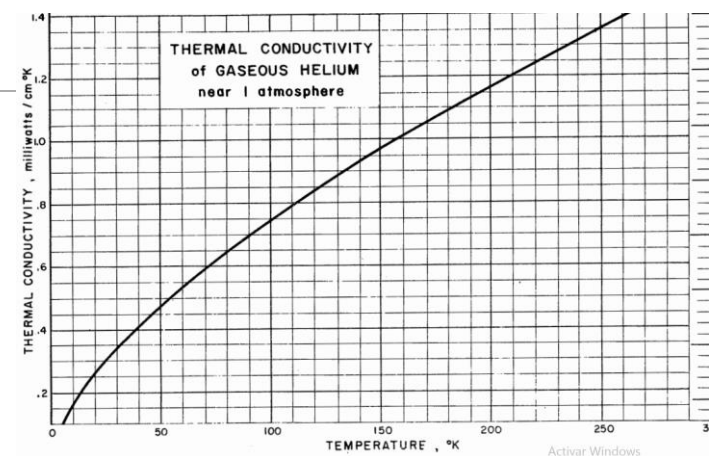
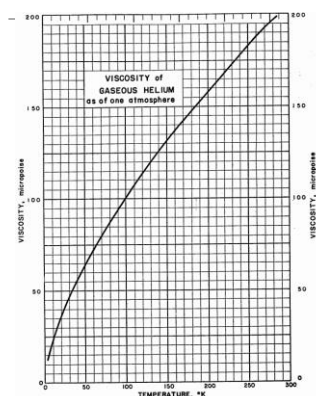
Constant Heat Capacity



Thermal Conductivity

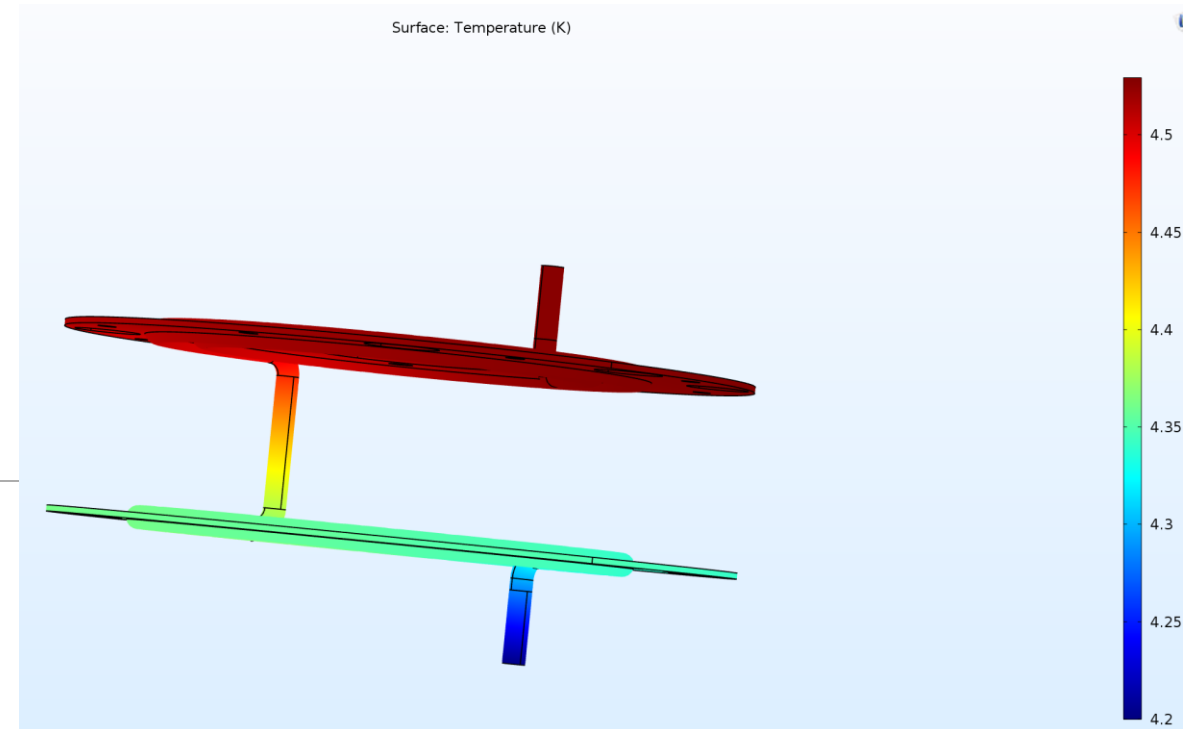
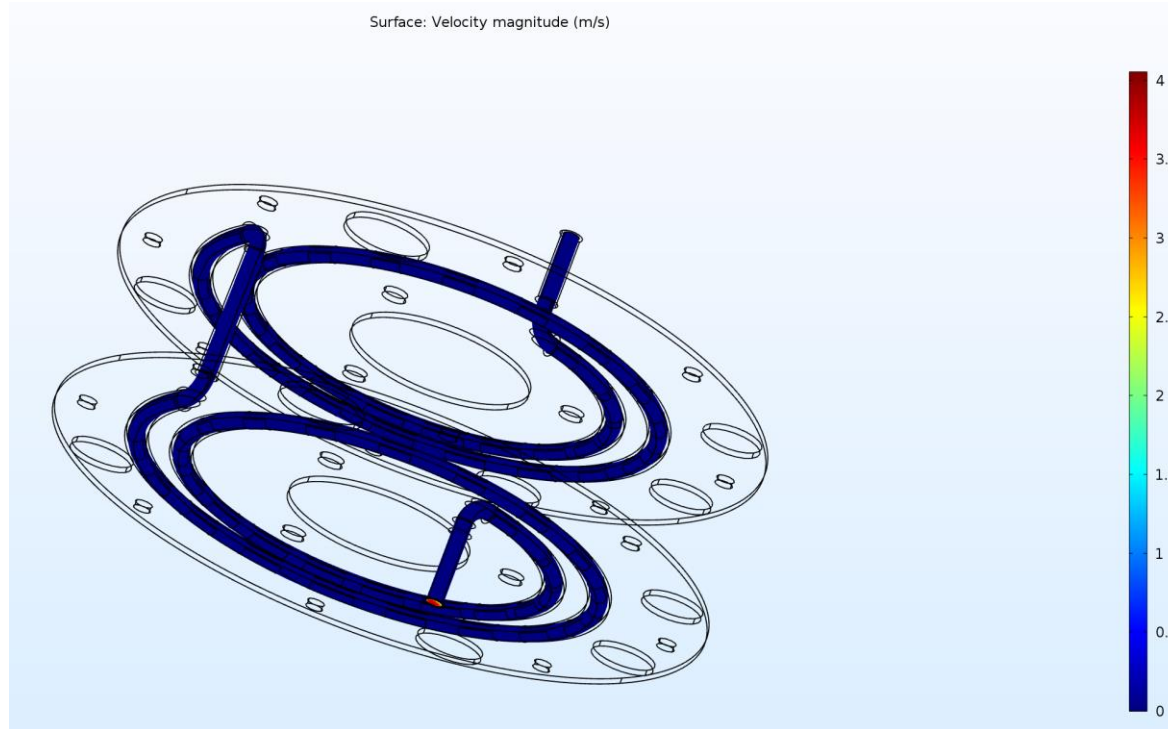


[4]



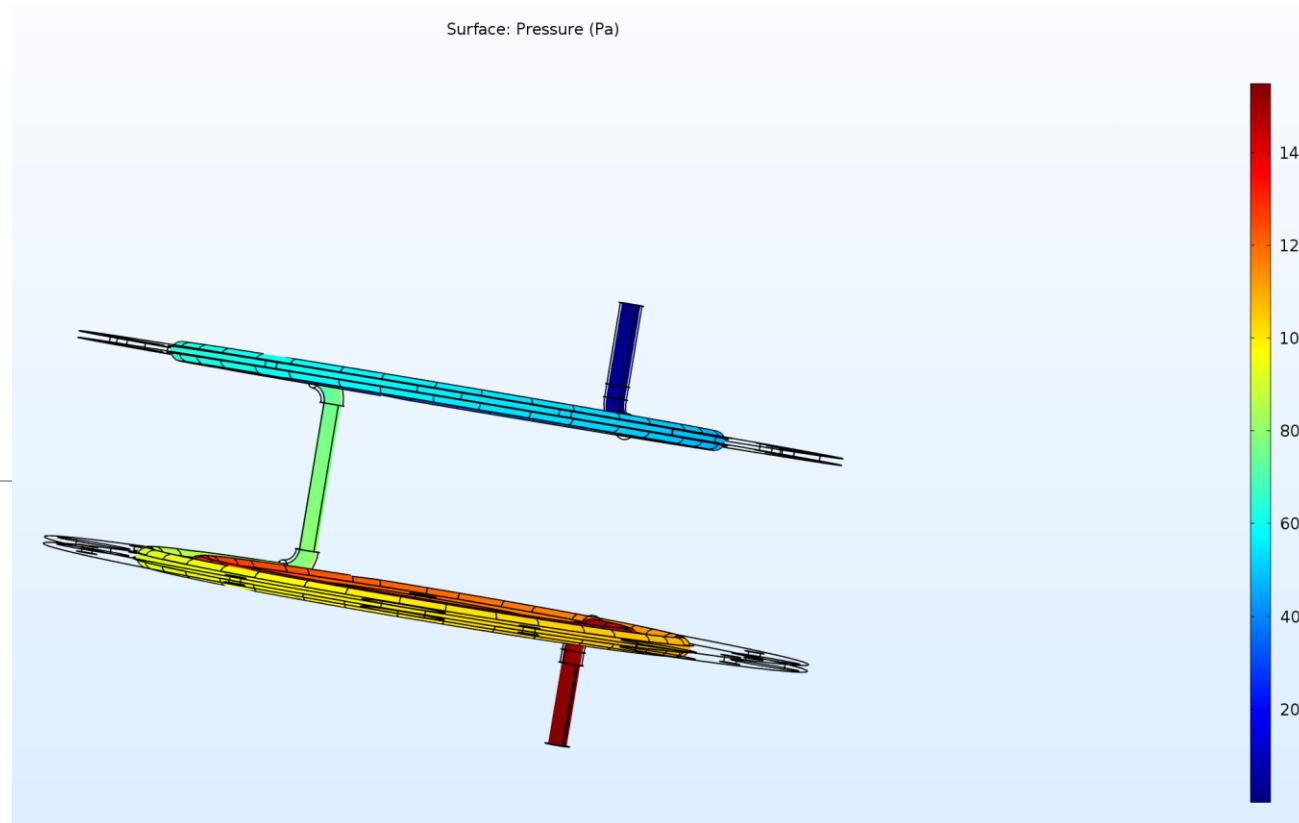
* With Ideal Gas :Density

0.1 W overall (16 SLPM) $T_{in}=4.2$ K

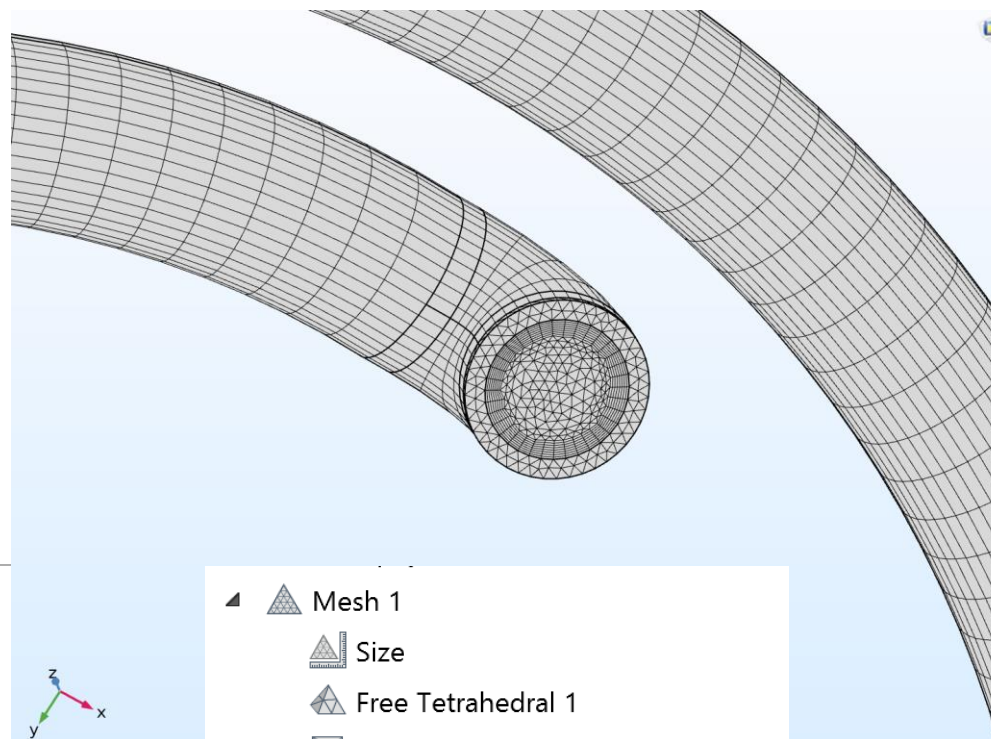
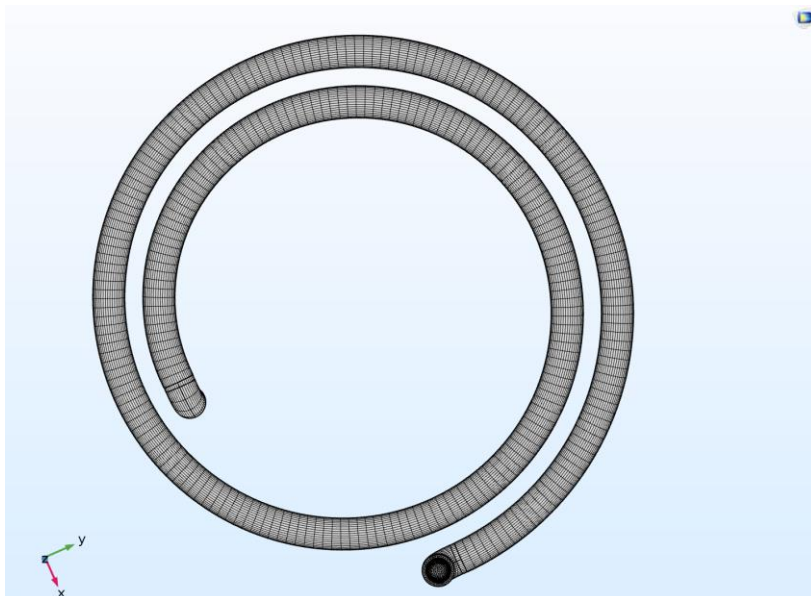


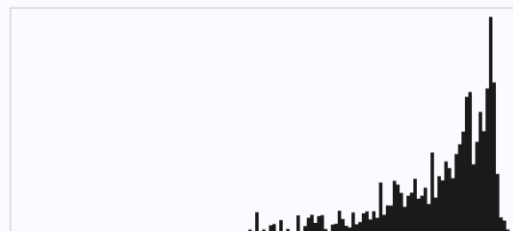
Baffles & HE Modeling: Pumped Helium

- First Evaporation Fridge Cool-Down

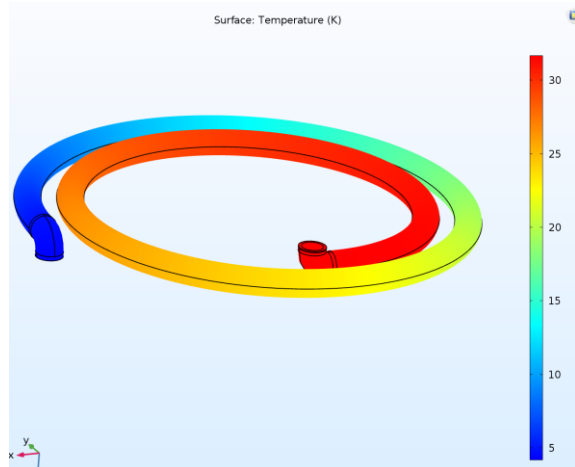


Baffles & HE Modeling: Mesh Improvement



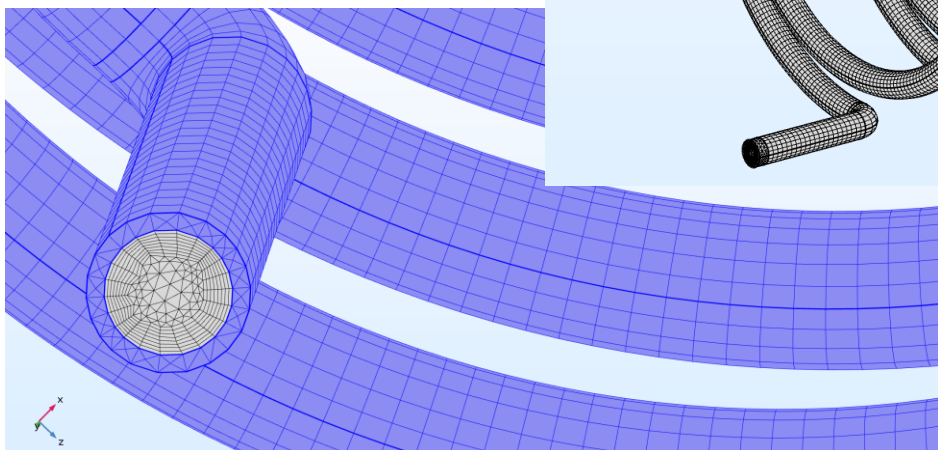
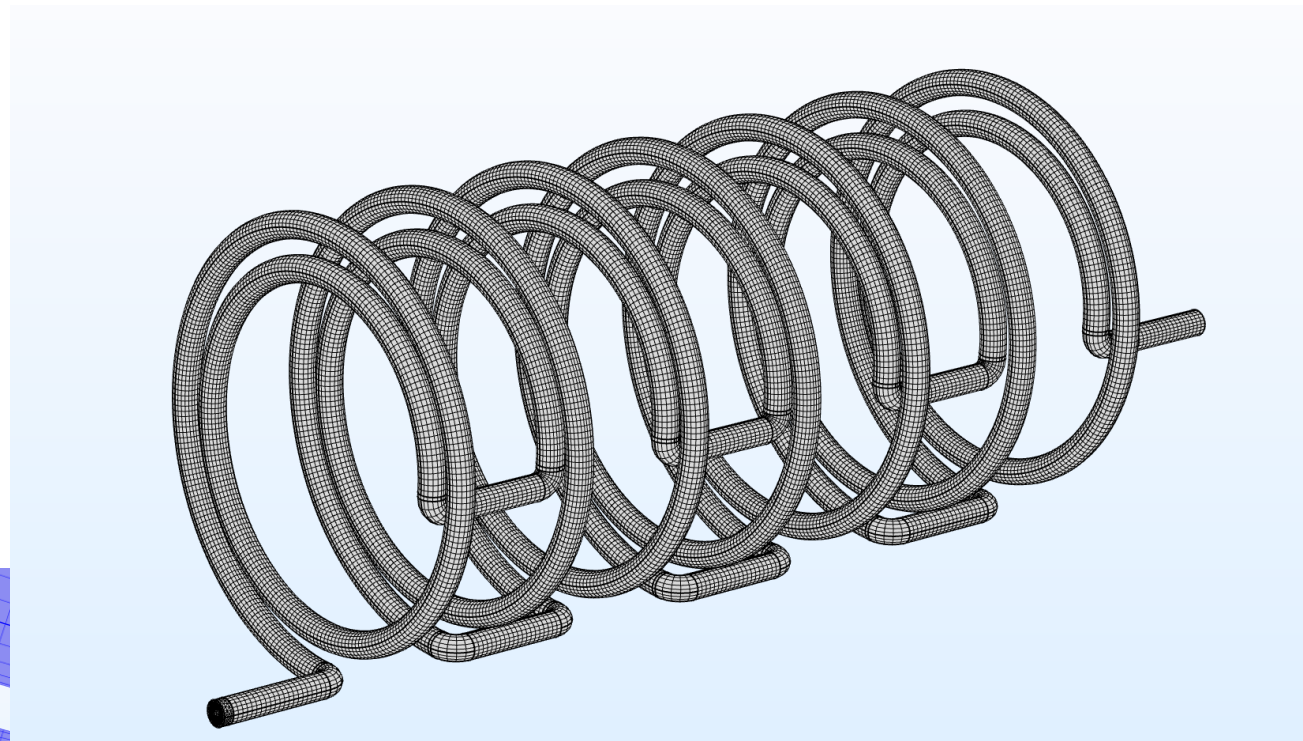
Element Quality	
Quality measure:	Skewness
Statistics	
Complete mesh	
Mesh vertices:	156167
Element type:	All elements
Tetrahedral elements:	1317
Prism elements:	132054
Hexahedral elements:	82416
Triangular elements:	1445
Quadrilateral elements:	24458
Edge elements:	1919
Vertex elements:	61
Domain element statistics	
Number of elements:	215787
Minimum element quality:	0.2239
Average element quality:	0.8124
Element volume ratio:	0.005385
Mesh volume:	34480.0 mm ³
Element Quality Histogram	
	

- Mesh 1
 - Size
 - Free Tetrahedral 1
- Boundary Layers 1
 - Boundary Layer Properties
 - Distribution 1
 - Swept 1



Baffles & HE Modeling: Mesh Improvement

- ▲ Mesh 1
 - ▲ Size
 - ▲ Free Tetrahedral 1
 - ▲ Boundary Layers 1
 - ▲ Boundary Layer Properties
 - Distribution 1
 - Swept 1



Element Quality

Quality measure:

Statistics

Complete mesh

Mesh vertices: 180420

Element type:

Tetrahedral elements: 0

Prism elements: 228456

Hexahedral elements: 0

— Domain element statistics

Number of elements: 228456

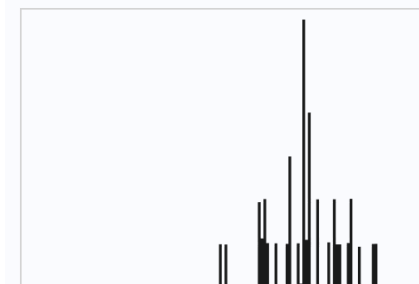
Minimum element quality: 0.4789

Average element quality: 0.6795

Element volume ratio: 0.07971

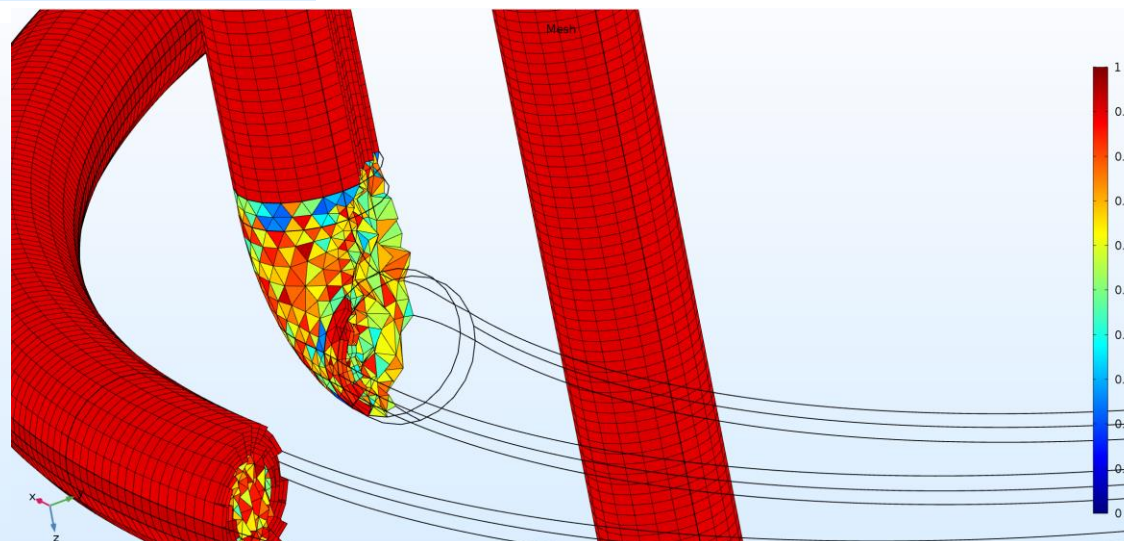
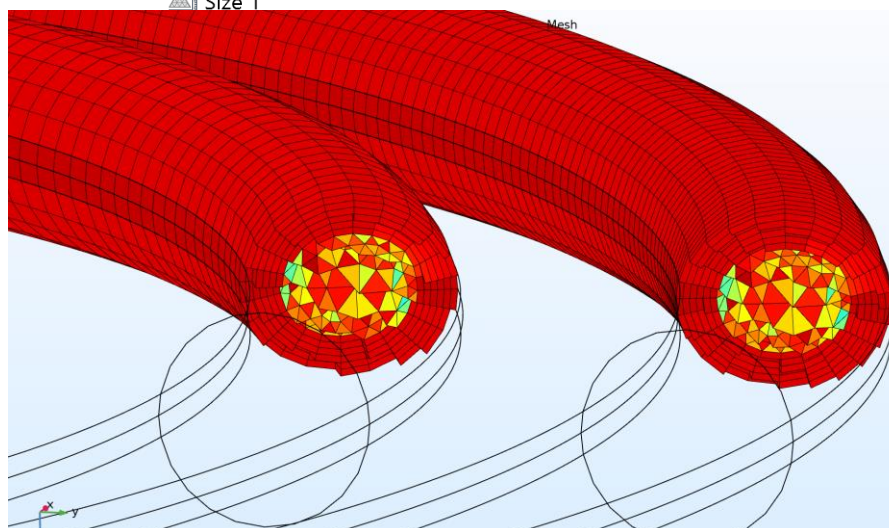
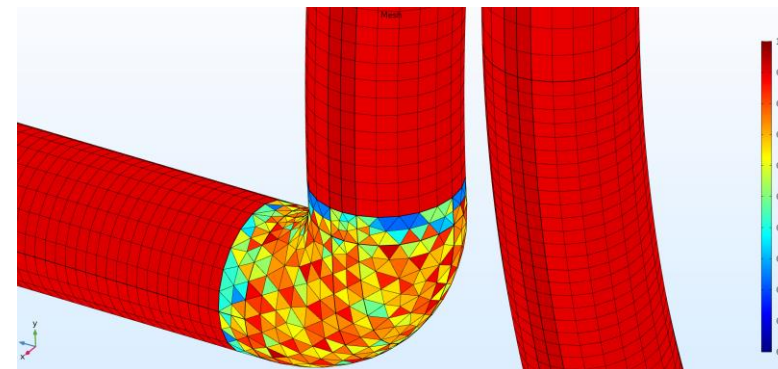
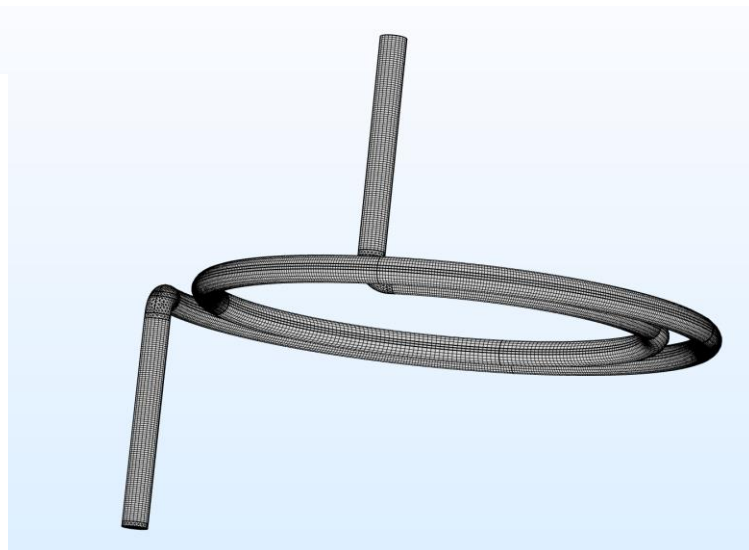
Mesh volume: 98090.0 mm³

Element Quality Histogram



Baffles & HE Modeling: Mesh Improvement

- Mesh 1
 - Size
 - Free Tetrahedral 1
 - Boundary Layers 1
 - Boundary Layer Properties
 - Swept 3
 - Distribution 1
 - Distribution 1
 - Swept 1
 - Copy Face 1
 - Swept 2
 - Free Tetrahedral 3
 - Size 1



Statistics

Partial mesh

Mesh vertices: 230741

Element type:

Tetrahedral elements: 12043

Pyramid elements: 552

Prism elements: 115636

Hexahedral elements: 156000

Triangular elements: 3044

Quadrilateral elements: 27812

Edge elements: 6354

Vertex elements: 84

— Domain element statistics

Number of elements: 284231

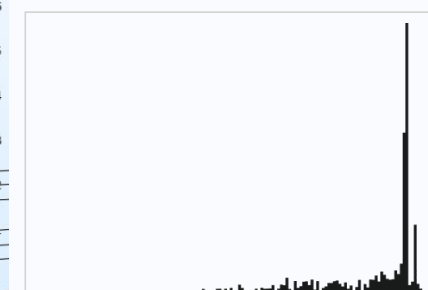
Minimum element quality: 0.1334

Average element quality: 0.8248

Element volume ratio: 0.001346

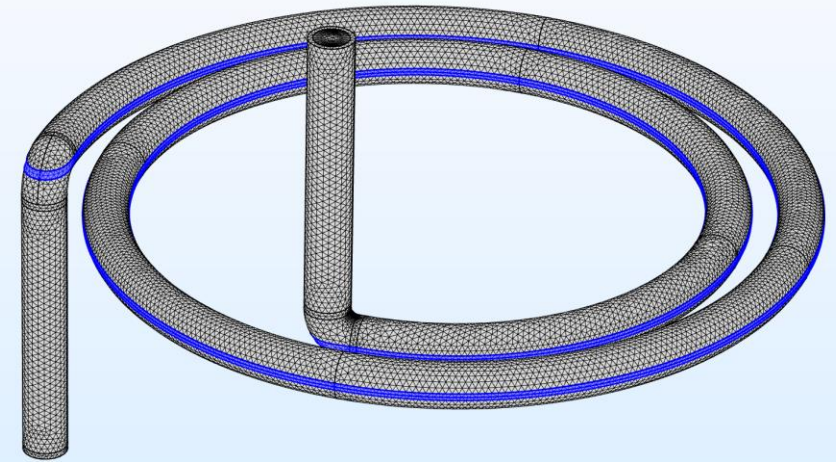
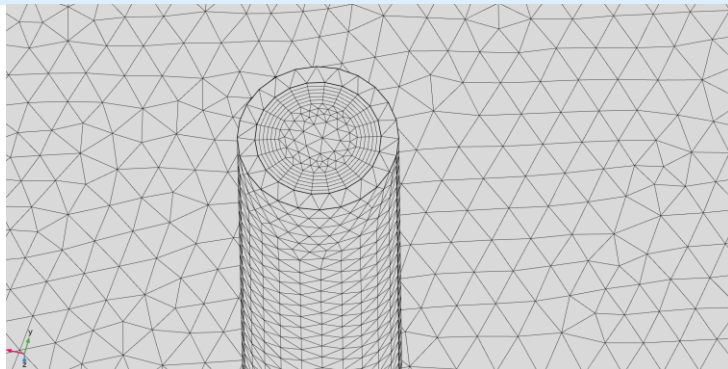
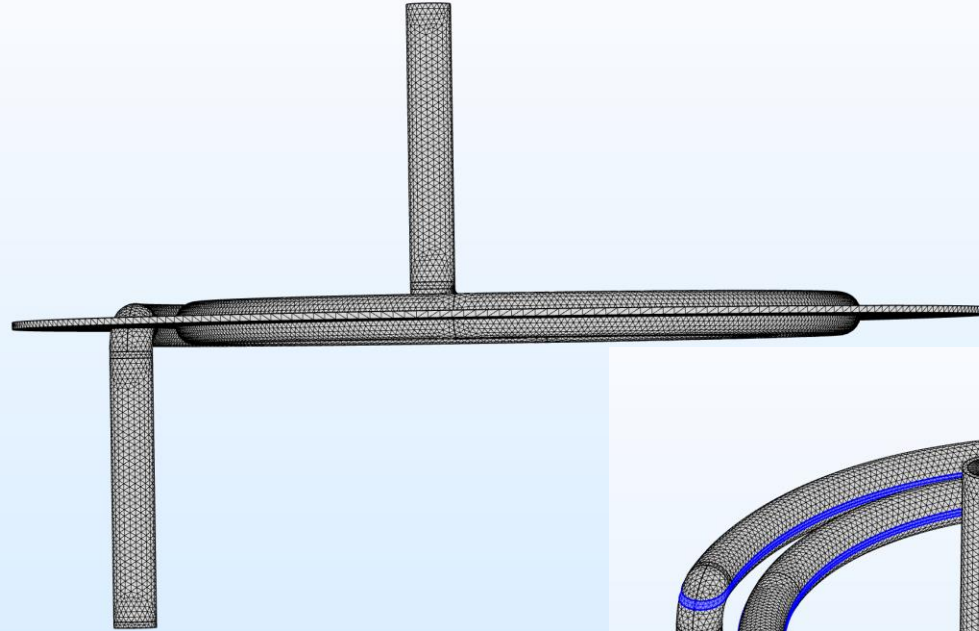
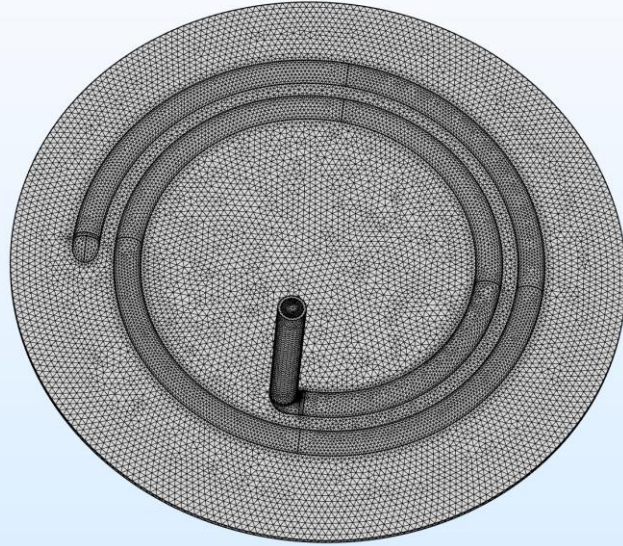
Mesh volume: 24060.0 mm³

Element Quality Histogram





Baffles & HE Modeling: Mesh Improvement



Baffles & HE Modeling: Incompressible NS with K-epsilon Turbulence model

Navier Stokes Equations with K-epsilon turbulent eddy viscosity model

$$\rho(\mathbf{u} \cdot \nabla)\mathbf{u} =$$

$$\nabla \cdot \left[-p\mathbf{I} + \left(\mu + \mu_T \right) (\nabla \mathbf{u} + (\nabla \mathbf{u})^T) \right] + \mathbf{F}$$

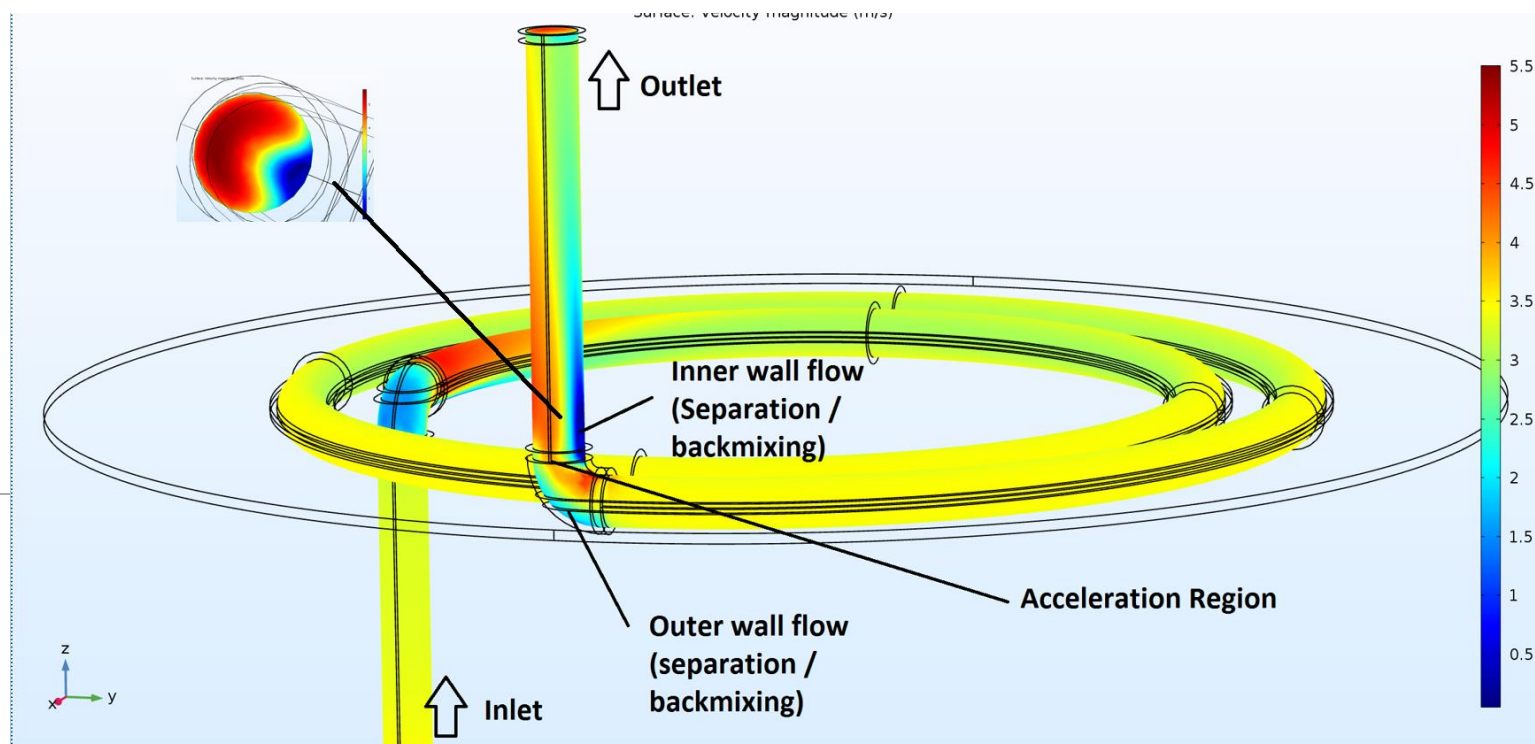
$$\rho \nabla \cdot (\mathbf{u}) = 0$$

$$\rho(\mathbf{u} \cdot \nabla)k = \nabla \cdot \left[\left(\mu + \frac{\mu_T}{\sigma_k} \right) \nabla k \right] + P_k - \rho \epsilon$$

$$\rho(\mathbf{u} \cdot \nabla)\epsilon = \nabla \cdot \left[\left(\mu + \frac{\mu_T}{\sigma_\epsilon} \right) \nabla \epsilon \right] + C_{\epsilon 1} \frac{\epsilon}{k} P_k - C_{\epsilon 2} \rho \frac{\epsilon^2}{k}, \quad \epsilon = \text{ep}$$

$$\mu_T = \rho C_\mu \frac{k^2}{\epsilon}$$

$$P_k = \mu_T \left[\nabla \mathbf{u} : (\nabla \mathbf{u} + (\nabla \mathbf{u})^T) \right]$$

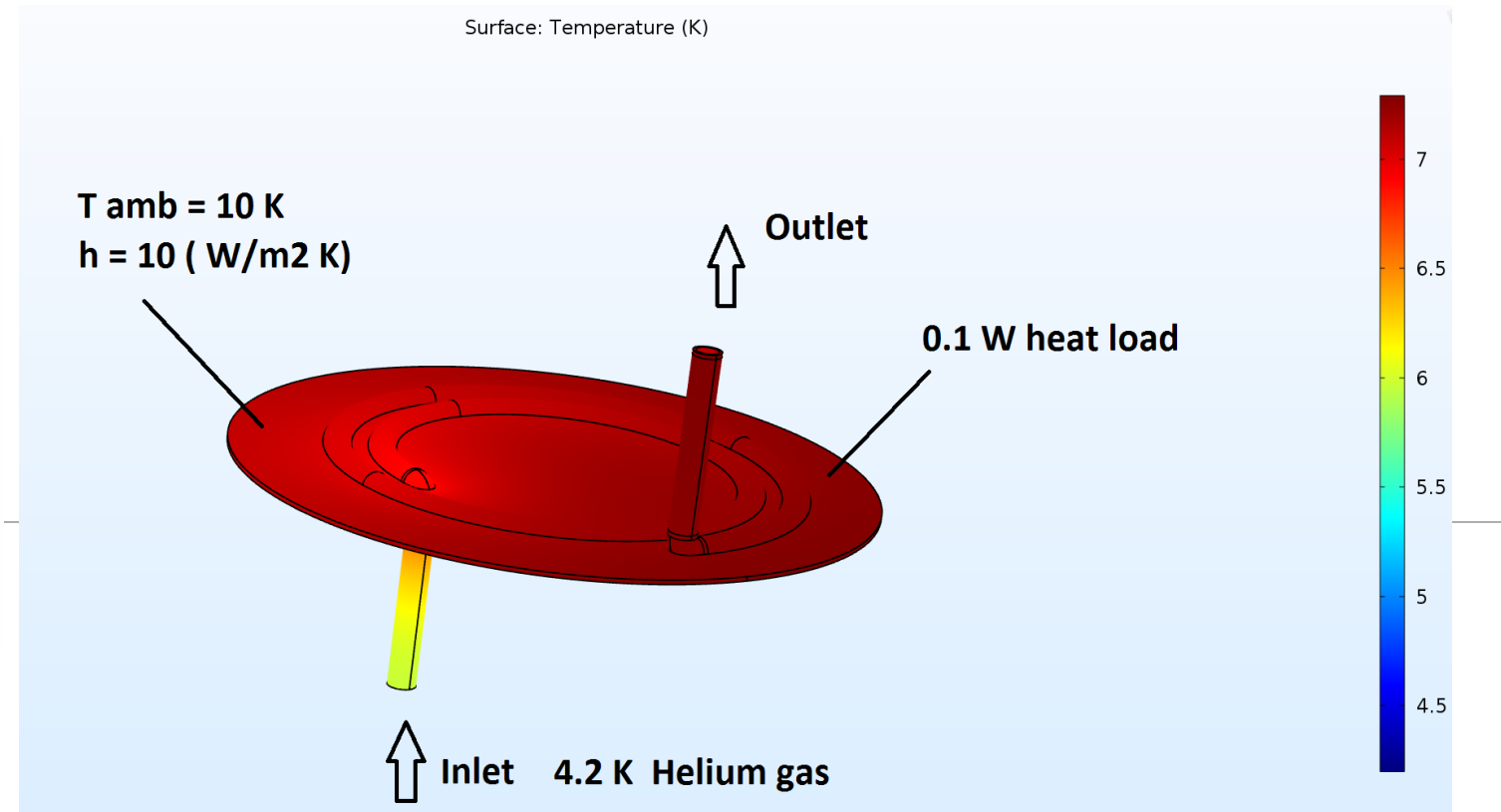


- Convective heat flux

$$q_0 = h \cdot (T_{\text{ext}} - T)$$

Table 1. Approximate values of heat transfer coefficient

Conditions of heat transfer	W/(m ² K)
Gases in free convection	5–37
Water in free convection	100–1200
Oil under free convection	50–350
Gas flow in tubes and between tubes	10–350
Water flowing in tubes	500–1200
Oil flowing in tubes	300–1700
Molten metals flowing in tubes	2000–45000
Water nucleate boiling	2000–45000
Water film boiling	100–300
Film-type condensation of water vapor	4000–17000
Drops size condensation of water vapor	30000–140000
Condensation of organic liquids	500–2300



Baffles & HE Modeling: Measurement Points

Rank of priority:

*** Very necessary

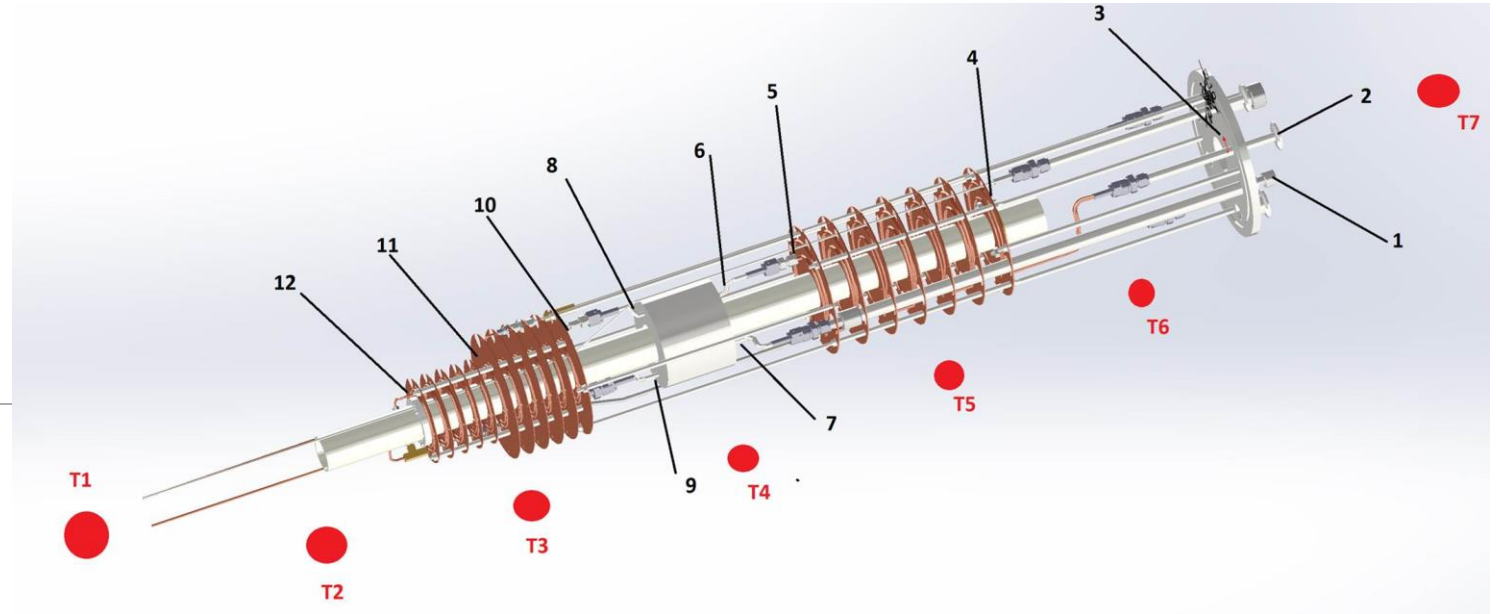
** Necessary

* Not that all (could be supposed)

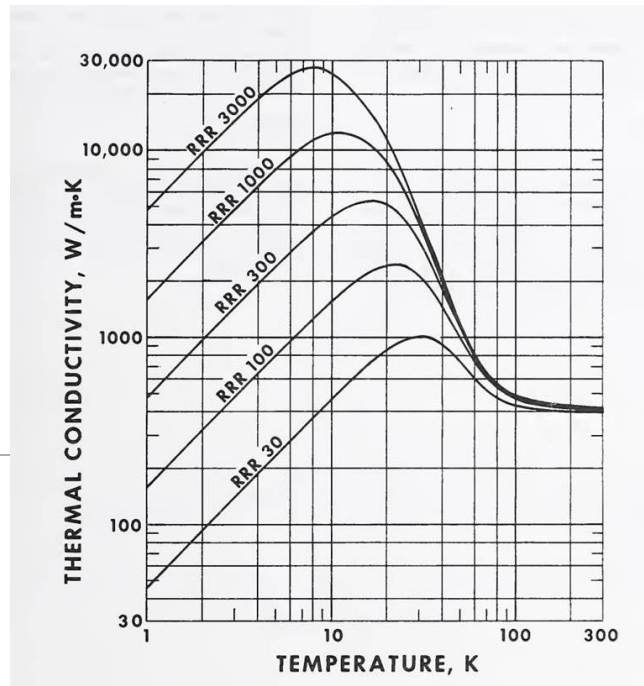
Point Description:

- 1) Helium inlet (mixture) : *** Mass flow (LPM), ***Temperature.
- 2) Helium outlet (gas): ***Vacuum pressure, ***Speed Pump(LPM), ***Temperature.
- 3) **Flange top Inner wall Temperature
- 4) ***Baffle outer wall temperature
- 5) ***Baffle lower wall temperature
- 6) Separator gas outlet : *Temperature
- 7) Separator Mixture inlet: *Temperature
- 8) Separator Liquid Bypass Outlet: **Temperature.
- 9) Separator Liquid Outlet: ***Temperature, ***mass flow.
- 10) ***HE outer wall temperature.
- 11) ***HE lower wall temperature
- 12) ***HE low low temperature wall.

Temperature Zones (red points) : ** Locally Wall
or Vapor bed Temperature measurements



RRR



Properties of copper change a lot depending on its purity, and also if it is immersed in to a magnetic field. The purity of free oxygen copper is measured by the value RRR, which means Residual Resistivity Ratio. This quantity is calculated as the ratio of electrical resistivity at 273K to the resistivity at 4 K. The RRR gives a measure of purity And the extent of physical defects such as lattice imperfections due to cold-working also electrical resistivity is function of the chemical and physical imperfection of the material.

Vacuum Viscous Flow Modeling

Main free path Helium

Mean Free Path Calculator

radius of molecule, $r =$ 130 pm

Temperature, $T =$ 4,2 K

Pressure, $P =$ 0,03 Kpa

(It is assumed that all particles are spherical !!!)
diameter of molecule, $d =$ 0,260 nm

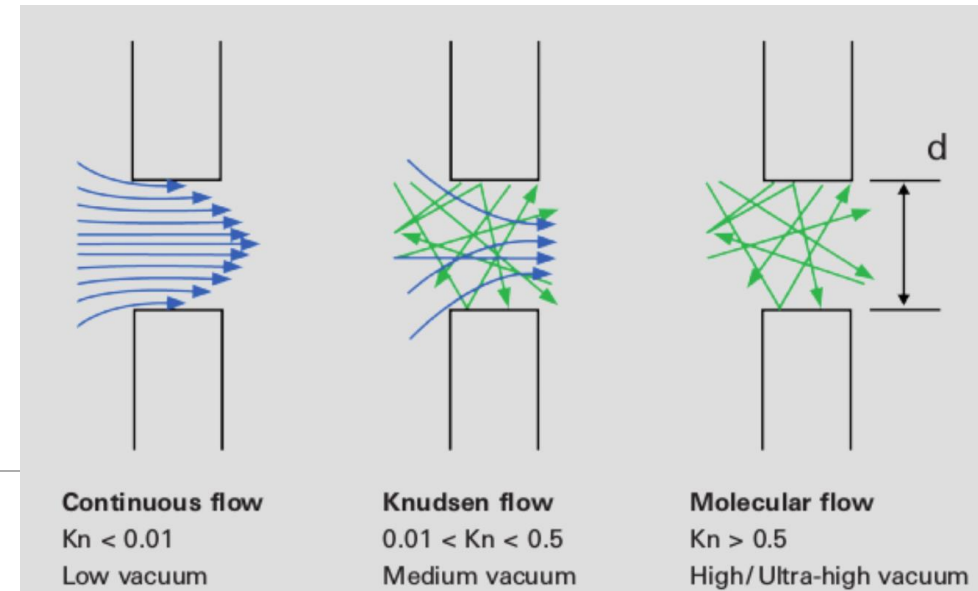
mean free path, $\lambda =$ 6,44E-06 m 6437,39 nm

$$\ell = \frac{k_B T}{\sqrt{2} \pi d^2 p},$$

$$Kn = \frac{\bar{\ell}}{d}$$

For 6 [mm] channel **Kn = 0,001073**

Continuous Flow



Laminar Compressible Flow CFD Modeling

2D Axisymmetric Domain

Fluid: Air

BC in = Mass Flow Inlet [6 m³/s]

BC outlet = Mass Flow Inlet [6 m³/s]

Initial Pressure field = 300 [Pa] (2.25 [Torr])

For pipe Flow:

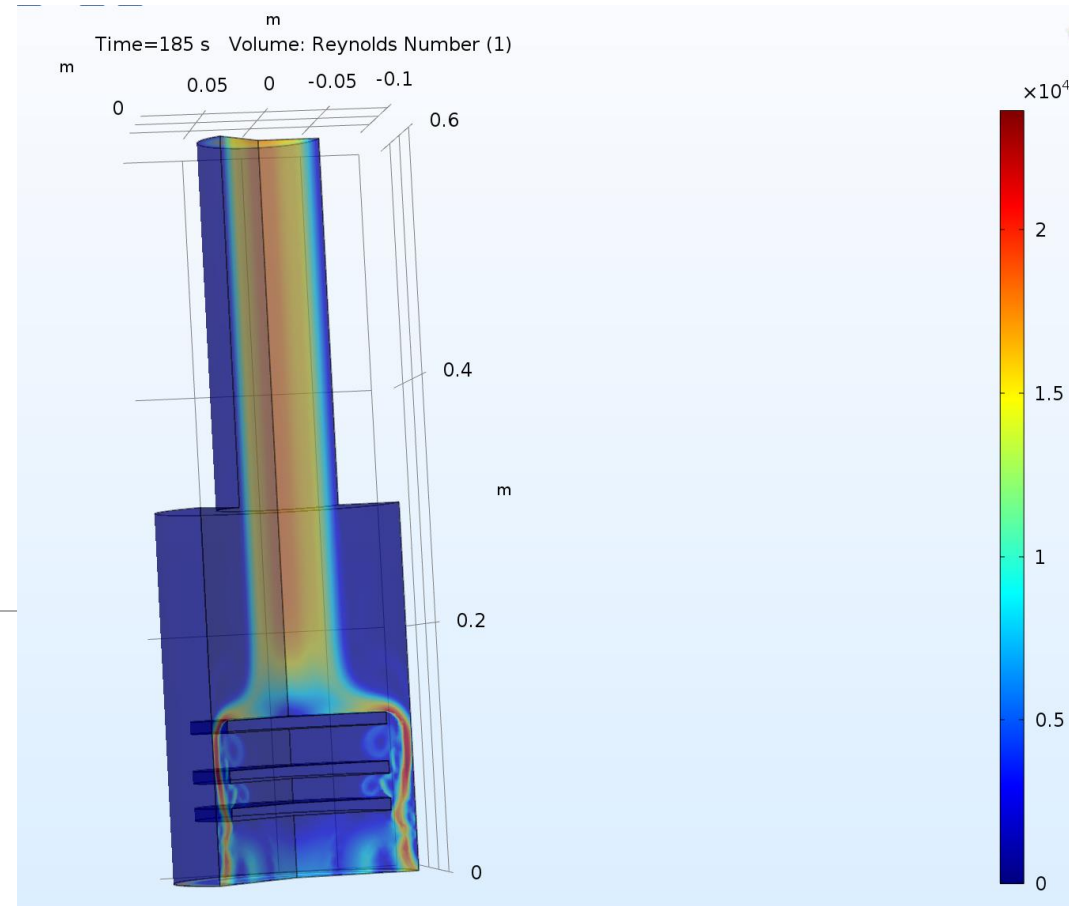
For $Re < 2000$ the flow is laminar

For $4000 > Re > 2000$ the flow is transient

For $Re > 4000$ the flow is turbulent

$$Re = \frac{\rho VL}{\mu} = \frac{VL}{\nu}$$

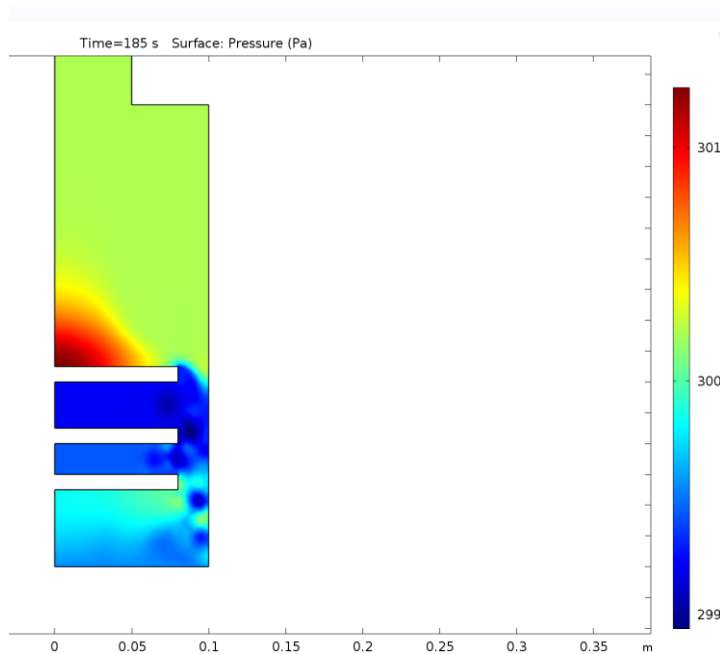
$$Re = \frac{F_{inertia}}{F_{viscous}} = \frac{\frac{kg}{m^3} \times \frac{m}{s} \times m}{Pa \times s} = \frac{F}{F}$$



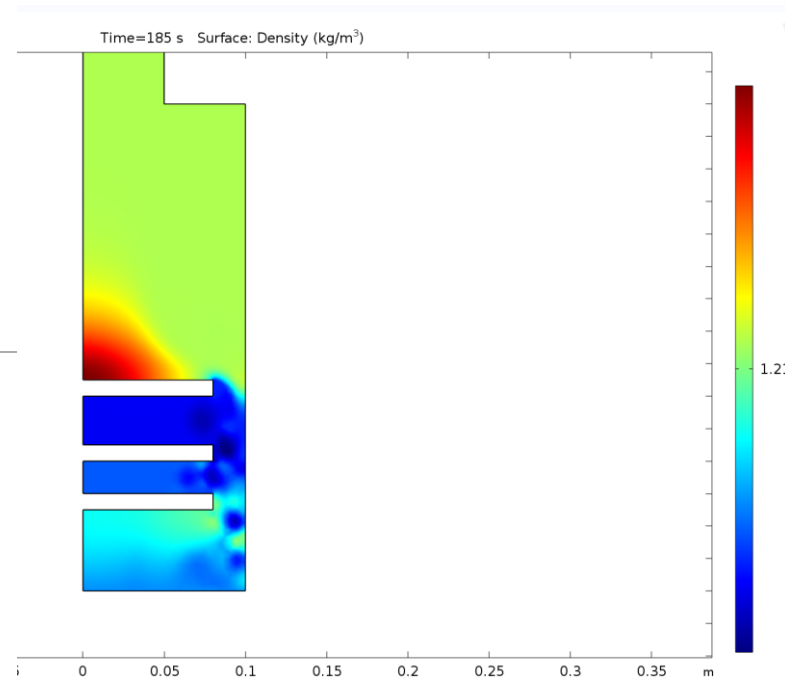
Compressible Flow

Pressure

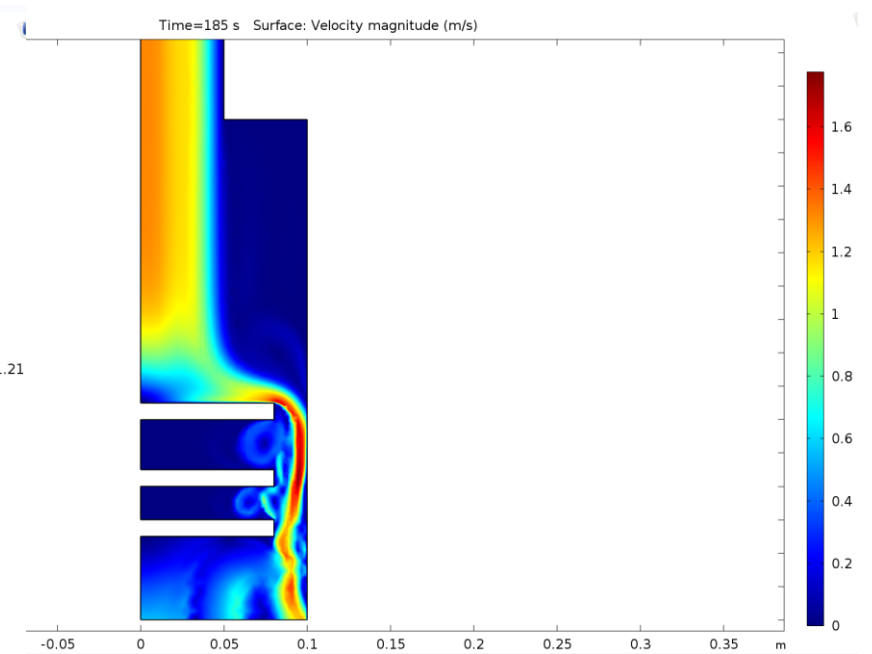
Pressure Drop: 2.32 [Pa]
(17[mTorr])



Density



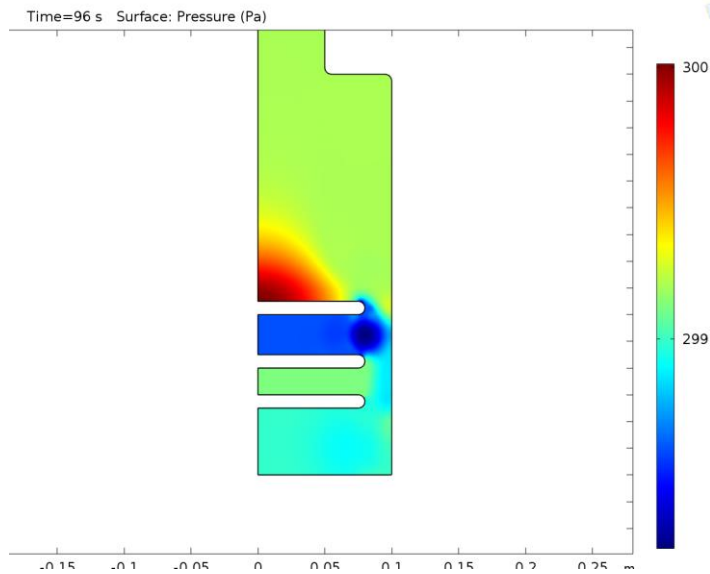
Velocity



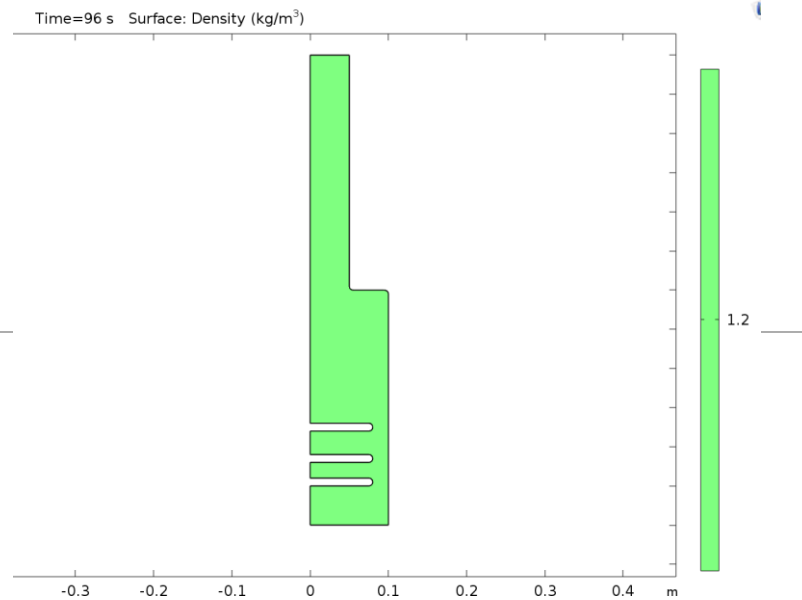
Vacuum Viscous Flow Modeling

Incompressible Flow (Change of P outlet BC=299 Pa)

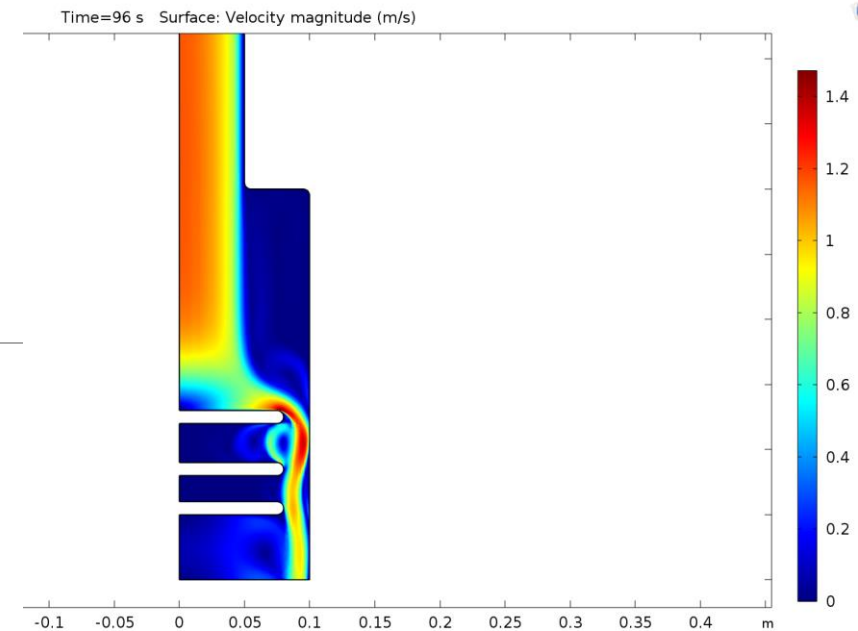
Pressure



Density



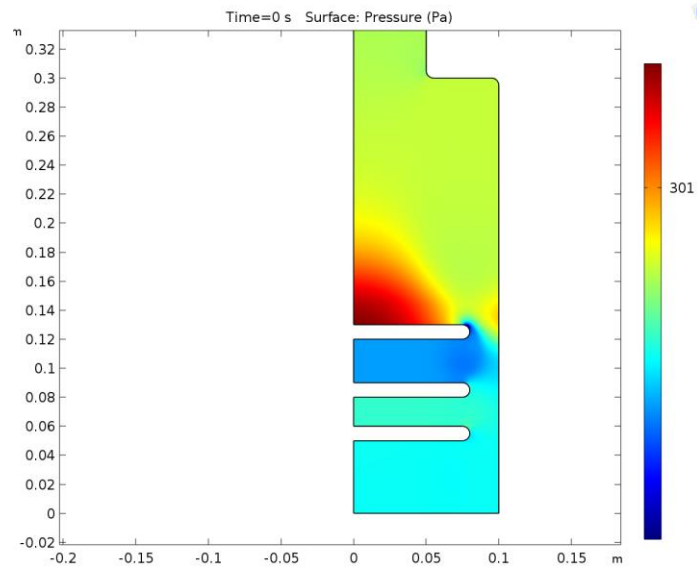
Velocity



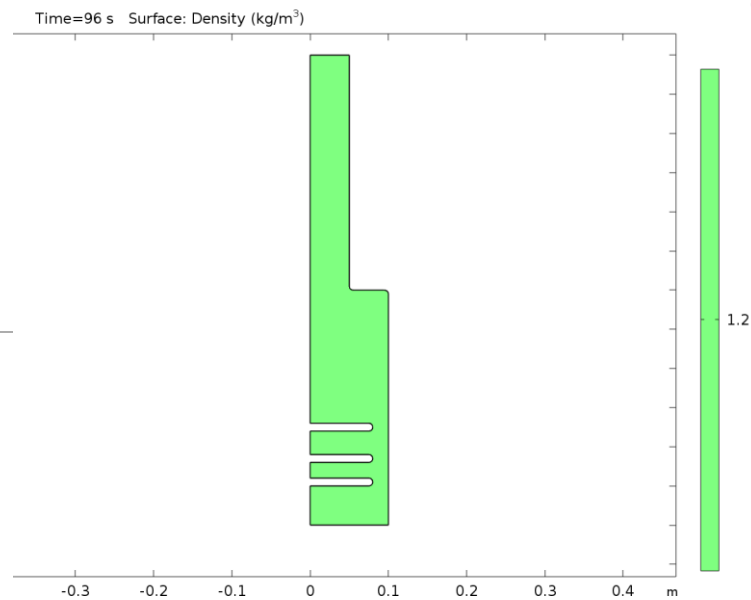
Vacuum Viscous Flow Modeling

Stationary K-e Turbulent Compressible Flow

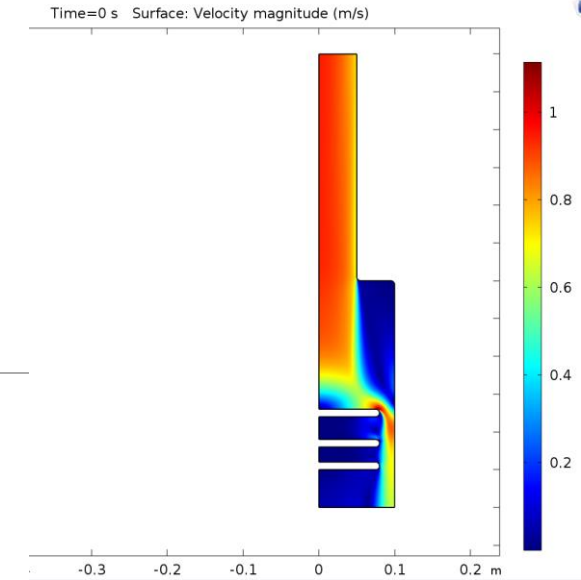
Pressure



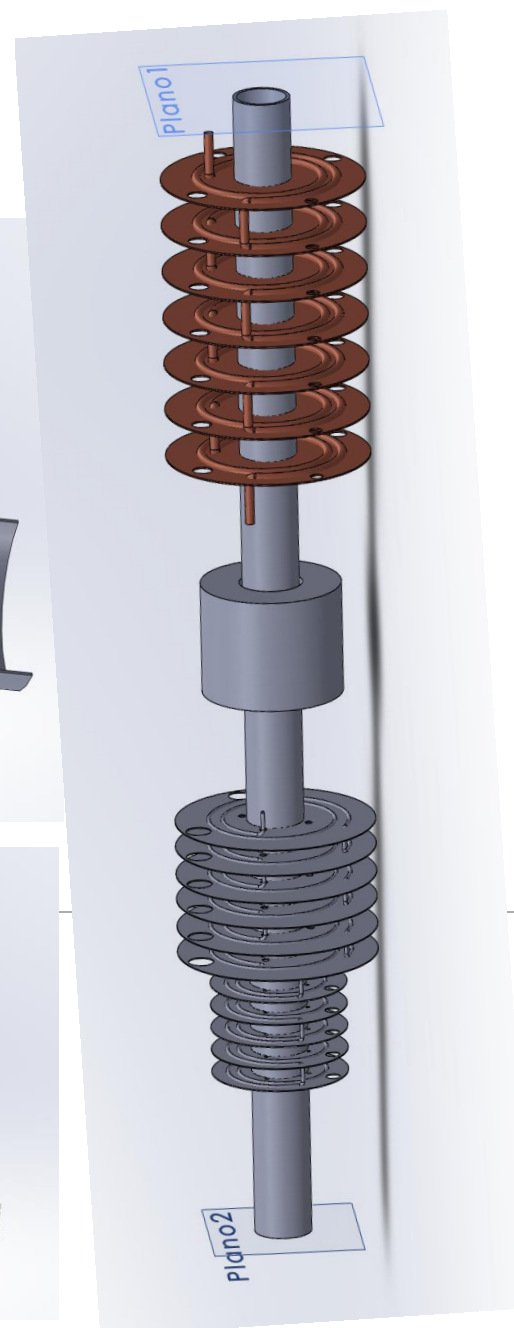
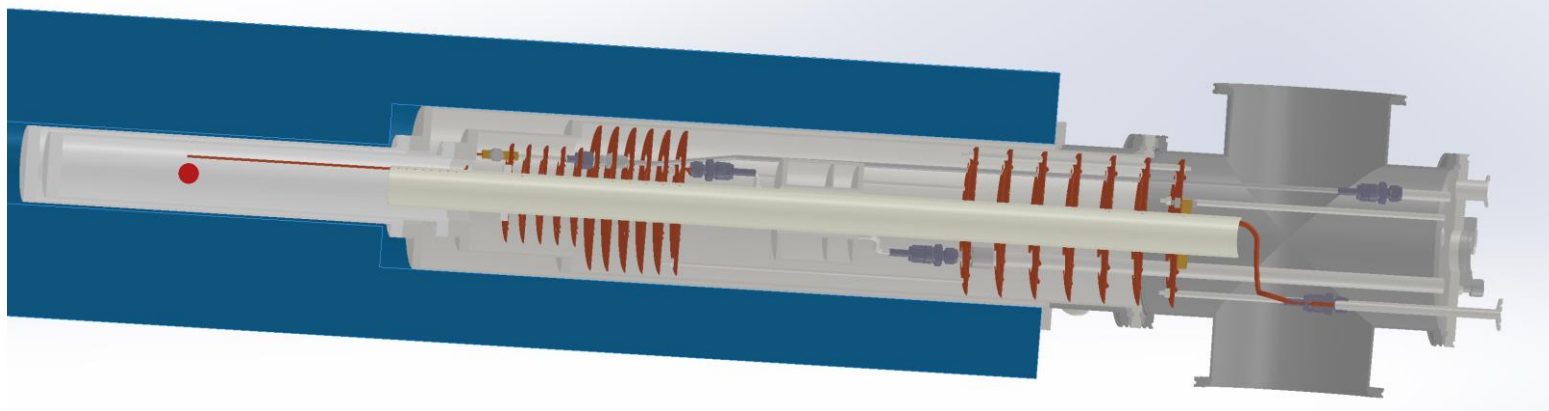
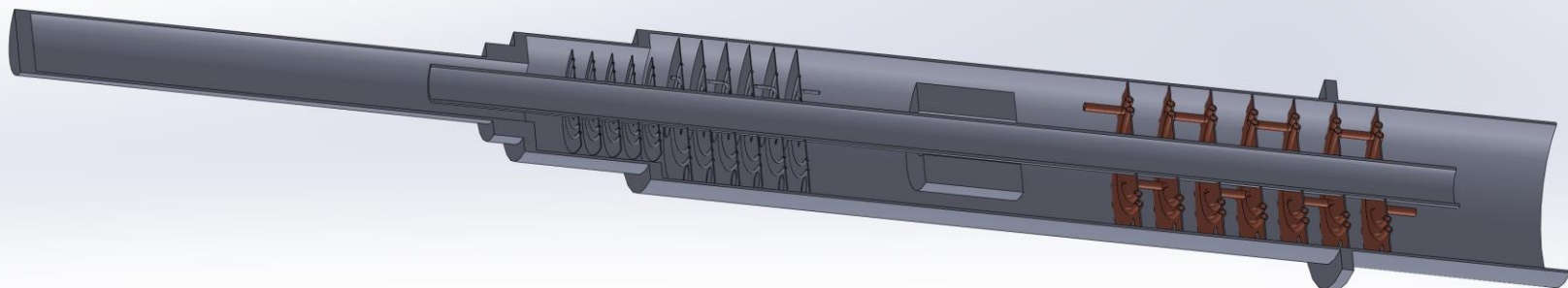
Density



Velocity



CAD Modeling



The Mesh

